#### Research Article

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# Influence of variable fluid properties on mixed convective Darcy-Forchheimer flow relation over a surface with Soret and Dufour spectacle

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Abstract: The thermo-diffusion applications of nanofluid subject to variable thermal sources have been presented. The significance of Darcy-Forchheimer effects is attributed. The flow comprises the mixed convection and viscous dissipation effects. Furthermore, the variable influence of viscosity, thermal conductivity, and mass diffusivity is treated to analyze the flow. The analysis of problem is referred to convective mass and thermal constraints. The analytical simulations are proceeded with homotopy analysis method. The convergence region is highlighted. Novel physical contribution of parameters is visualized and treated graphically. It is noted that larger Brinkman number leads to improvement in heat transfer. The concentration pattern boosted due to Soret number. The wall shear force enhances with Hartmann number and variable thermal conductivity coefficient.

**Keywords:** Darcy–Forchheimer model, Soret and Dufour phenomenon, convective temperature and concentration constraints, variable transport characteristics

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## 1 Introduction

The nanomaterials are treated as an improved source of energy as a liquid in different industrial processes. The decomposition of nanofluids preserves peak thermal concavity and other features. Various applications of nanomaterials are observed in energy systems, chemical reactions, nuclear systems, high-energy physics, radiative phenomenon, etc. Different studies are performed by many researchers for nanofluids. Wang et al. [1] observed the graphene nanoparticles to boost the performances of engine oil with additional melting phenomenon. The ciliated wavy surface flow comprising the nanofluid endorsing the physiological properties was observed by Fuzhang et al. [2]. Imtiaz et al. [3] developed the understanding of magnetic dipole for nanofluid problem with diverse thermal properties. Wang et al. [4] presented the reflection of solar energy performances with nanoparticle applications. Jayadevamurthy et al. [5] emphasized toward the bioconvective phenomenon due to hybrid nanofluid in rotating systems. Wang et al. [6] observed the natural convective nanofluid flow under the role of chemotaxis phenomenon. Li et al. [7-10] explored the fluid flow behavior in the presence of various boundary constraints.

Thermo-diffusion, also known as the Soret effect, is a process where solutes are transported in a medium due to a thermal gradient. Most solutes have positive coefficients, indicating that they will diffuse down the thermal gradient, away from the heat source. However, some solutes have negative coefficients and may move up the gradient. The Soret coefficients for various solutes can be found in the study by de Marsily *et al.* [11]. The importance of thermo-diffusion in the disposal of heat-emitting waste in pelagic silts has been investigated by Thornton and Seyfried [12]. It was noted that the thermo-diffusion plays a significant role in this process. Idowu and Falodun [13] claimed the vertical flow due to thermo-diffusion transport under the Newtonian heating. Javed *et al.* [14] evaluated the Dufour consequences for numerically treated viscoelastic fluid. Li *et al.* [15]

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highlighted the Soret and Dufour appliances for optimized flow. Suchana  $et\ al.$  [16] visualized the multi wall carbon nanotubes- $H_2O$  decomposition in an L-shaped configuration. The Carreau nanofluid with Soret interaction was determined by Salahuddin  $et\ al.$  [17]. Mng'ang'a and Richard Onyango [18] examined the Couette flow due to Jeffrey fluid via inclined channel. Yang  $et\ al.$  [19] and Sun  $et\ al.$  [20] investigated heat flow  $via\ 3D$ -printed thermal meta-materials and shear-thickening fluids based on carbon fiber and silica nanocomposite, respectively.

The study of fluid flow through porous saturated spaces is crucial in various fields such as geophysics, petroleum engineering, industrial geophysics, geothermal operations, soil sciences, packed filters, and ion-exchange columns. Porous media consist of tiny pores through which fluids can be absorbed or injected. These media find applications in energy storage, oil filtration, and thermal receivers. The Darcy law is associated with the applications of porous media in the absence of inertial forces [21-25]. However, this law has limitations in validating low velocity ranges and small porosity spaces. To address this issue, the non-Darcian porous medium, known as the Darcy-Forchheimer law, provides a generalized approach to studying porous spaces, even at low porosity levels. This law successfully describes inertial features, variable porous effects, and boundary impacts. In recent studies, researchers have been exploring the application of the Darcy-Forchheimer model to porous medium flow problems. Ullah et al. [26] investigated the influence of lip on rotating disk flow with nanoparticles using this model. Siddiqui et al. [27] numerically focused on the Casson particles and optimized the determination using the Darcy-Forchheimer model. Saini et al. [28] discussed the modified Darcy contribution for the Jeffrey fluid in porous space with cylindrical particles. Alzahrani and Khan [29] investigated the impact of activation energy on three-dimensional Darcy-Forchheimer flow patterns. Li et al. [40] examined that the unsteady fluid flow and heat transport subject to generalized lie similarity transformations and thermal radiation.

The objective of present continuation is to analyze the thermo-diffusion mixed convection flow of nanofluid comprising the variable thermal sources. The novel features of current work are:

- A mixed convection flow of nanofluid with variable viscosity endorsing by moving stretched surface is analyzed,
- The flow is subject to significance of Darcy–Forchheimer phenomenon,
- The viscous dissipated impact is utilized,
- The Soret and Dufour features are contributed,
- The dealing of heat transfer is preserved under the assumptions of variable thermal conductivity,

- The objective of nanofluid concentration is attained with chemical reaction outcomes,
- Both mass and heat fluctuated assessment are inspected with convective transport constraints,
- Computational results for modeled problem were computed *via* homotopy analysis method (HAM) [30–32].

It is remarked that different studies are recently summarized for studying various aspects of nanomaterials. However, analysis for Darcy–Forchheimer flow of nanofluid with variable thermal features and thermo-diffusion effects has not been focused yet. Current model aims to fulfill this research gap. A physical attribution of problem is observed.

# 2 Formulation of problem

In this study, we investigate the two-dimensional, incompressible, steady mixed convective flow of a viscous fluid over a movable surface in the presence of Soret and Dufour effects. The flow takes place in a Darcy–Forchheimer porous medium with variable transport characteristics, including thermal conductivity, viscosity, and diffusivity. The temperature and concentration distributions are determined, considering the effects of thermophoresis and Brownian diffusion. Additionally, convective boundary conditions for temperature and concentration are applied at the surface boundary. The surface is stretched having velocity  $(u_w(x) = ax)$  with a > 0. A constant magnetic is applied with constant strength  $(B_0)$ . The physical representation of the flow is shown in Figure 1.

Governing equations are as follows [33–36]:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0, (1)$$

$$\rho_{\rm f} \left[ u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right] = \frac{\partial}{\partial y} \left[ \mu(T) \frac{\partial u}{\partial y} \right] - \sigma_{\rm f} B_0^2 u - \frac{\mu_{\rm f}}{k_{\rm p}} u - \rho_{\rm f} F u^2$$

$$+ g^* \rho_{\rm f} \beta^* (T - T_{\infty}) + g^* \rho_{\rm f} \beta^{**} (C - C_{\infty})$$
(2)

$$u\frac{\partial T}{\partial x} + v\frac{\partial T}{\partial y} = \frac{1}{(\rho c_{\rm p})_{\rm f}} \frac{\partial}{\partial y} \left[ k(T) \frac{\partial T}{\partial y} \right] + \tau \left[ D_{\rm b} \frac{\partial C}{\partial y} \frac{\partial T}{\partial y} + \frac{D_{\rm T}}{T_{\infty}} \left( \frac{\partial T}{\partial y} \right)^{2} \right] + \frac{\sigma_{\rm f} B_{\rm 0}^{2}}{(\rho c_{\rm p})_{\rm f}} u^{2} + \frac{D_{\rm b} k_{\rm T}}{(c_{\rm p})_{\rm f}} C_{\rm s} \frac{\partial^{2} C}{\partial y^{2}}$$
(3)

$$u\frac{\partial C}{\partial x} + v\frac{\partial C}{\partial y} = D_{\rm B}(C)\frac{\partial^2 C}{\partial y^2} + \frac{D_{\rm T}}{T_{\rm \infty}} \left(\frac{\partial^2 T}{\partial y^2}\right) + \frac{D_{\rm b}k_{\rm T}}{T_{\rm m}} \left(\frac{\partial^2 T}{\partial y^2}\right)$$
(4)
$$- k_{\rm r}^2(C - C_{\infty}),$$

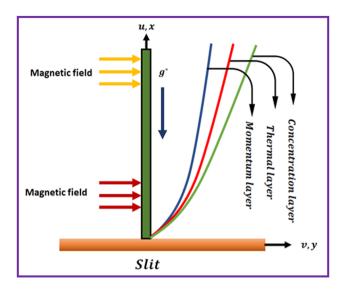


Figure 1: Flow sketch.

$$u = ax, \quad v = 0, \quad -k_{\rm f} \frac{\partial T}{\partial y} = h_{\rm f}(T_{\rm w} - T),$$

$$-D_{\rm B} \frac{\partial C}{\partial y} = h_{\rm w}(C_{\rm w} - C) \quad \text{at } y = 0$$

$$u \to 0, \ T \to T_{\infty}, C \to C_{\infty} \quad \text{as } y \to \infty$$

$$(5)$$

Here, (u, v) signify the velocity components,  $D_b$ Brownian motion coefficient,  $T_{\rm m}$  mean fluid temperature,  $\mu_{\rm f}$  dynamic viscosity,  $T_{\rm w}$  wall temperature,  $\sigma_{\rm f}$  electrical conductivity,  $\beta^*$  thermal expansion coefficient, (x, y) Cartesian coordinates,  $h_{\rm f}$  heat transfer rate,  $g^*$  gravity,  $\rho_{\rm f}$  density of fluid,  $\beta^{**}$  the solutal expansion coefficient, T temperature,  $F = \frac{C_b}{k_c}$  non-uniform inertia coefficient,  $(c_p)_f$  specific heat, l

characteristics length,  $k^*$  mean absorption coefficient,  $k_r^2$ reaction rate,  $\tau$  the ratio of heat capacitance,  $k_p$  porous space coefficient,  $k_{\rm T}$  thermal diffusion ratio,  $T_{\infty}$  ambient temperature,  $h_{\rm w}$  mass transfer rate,  $\sigma^*$  Stefan–Boltzmann constant,  $C_{\rm s}$  concentration susceptibility,  $D_{\rm T}$  thermophoresis coefficient,  $k_{\mathrm{f}}$  thermal conductivity, C the concentration,  $C_{\mathrm{w}}$ wall concentration, and  $C_{\infty}$  ambient concentration. Here, variable fluid behaviors are defined as [37,38]:

$$\mu(T) = \mu_{\rm f} \left[ 1 + \epsilon_1 \left( \frac{T - T_{\infty}}{T_{\rm w} - T_{\infty}} \right) \right],$$
 (6)

$$k(T) = k_{\rm f} \left[ 1 + \epsilon_2 \left[ \frac{T - T_{\infty}}{T_{\rm W} - T_{\infty}} \right] \right], \tag{7}$$

$$D_{\mathrm{B}}(C) = D_{\mathrm{b}} \left[ 1 + \epsilon_{3} \left[ \frac{C - C_{\infty}}{C_{\mathrm{w}} - C_{\infty}} \right] \right]. \tag{8}$$

Using transformations [39]

$$u = x \frac{\partial f(\xi, \eta)}{\partial \eta},$$

$$v = -\sqrt{av_{\rm f}} \left\{ f(\xi, \eta) + \xi \frac{\partial f(\xi, \eta)}{\partial \xi} \right\}, \quad \theta(\xi, \eta) = \frac{T - T_{\infty}}{T_{\rm w} - T_{\infty}}$$

$$\phi(\xi, \eta) = \frac{C - C_{\infty}}{C_{\rm w} - C_{\infty}}, \quad \xi = \frac{x}{l}, \quad \eta = \sqrt{\frac{a}{v_{\rm f}}} y$$

$$(9)$$

One can found that

$$(1 + \epsilon_{1}\theta)\frac{\partial^{3}f}{\partial\eta^{3}} + \epsilon_{1}\frac{\partial\theta}{\partial\eta}\frac{\partial^{2}f}{\partial\eta^{2}} + f\frac{\partial^{2}f}{\partial\eta^{2}} + \xi\frac{\partial f}{\partial\xi}\frac{\partial^{2}f}{\partial\eta^{2}} - \left(\frac{\partial f}{\partial\eta}\right)^{2}$$
$$-\xi\frac{\partial^{2}f}{\partial\xi\partial\eta}\frac{\partial f}{\partial\eta} - M\frac{\partial f}{\partial\eta} - \lambda\frac{\partial f}{\partial\eta} - \operatorname{Fr}\xi\left(\frac{\partial f}{\partial\eta}\right)^{2}$$
$$+\frac{\beta_{t}}{\xi}(\theta + \beta_{c}\varphi) = 0$$
 (10)

$$(1 + \epsilon_{2}\theta)\frac{\partial^{2}\theta}{\partial\eta^{2}} + \epsilon_{2}\left[\frac{\partial\theta}{\partial\eta}\right]^{2} + \Pr\left\{\frac{\partial f}{\partial\xi}\frac{\partial\theta}{\partial\eta} + \Pr\left\{\frac{\partial\theta}{\partial\eta}\right\}^{2}\right\} - \Pr\left\{\frac{\partial\theta}{\partial\xi}\frac{\partial f}{\partial\eta} + \Pr\left(\frac{\partial\theta}{\partial\eta}\right)^{2}\right\} + \Pr\left\{\frac{\partial\theta}{\partial\eta}\frac{\partial f}{\partial\eta} + \Pr\left(\frac{\partial\theta}{\partial\eta}\right)^{2}\right\} + M\operatorname{Br}\left\{\frac{\partial^{2}\theta}{\partial\eta^{2}}\right\}^{2} + \Pr\left(\frac{\partial^{2}\theta}{\partial\eta^{2}}\right)^{2} = 0$$

$$(11)$$

$$(1 + \epsilon_{3}\phi)\frac{\partial^{2}\phi}{\partial\eta^{2}} + \epsilon_{3}\left[\frac{\partial\phi}{\partial\eta}\right]^{2} + \operatorname{Sc} f\frac{\partial\phi}{\partial\eta} + \operatorname{Sc} \xi\frac{\partial f}{\partial\xi}\frac{\partial\phi}{\partial\eta} - \operatorname{Sc} \xi\frac{\partial\phi}{\partial\xi}\frac{\partial f}{\partial\eta} + \frac{\operatorname{Nt}}{\operatorname{Nb}}\frac{\partial^{2}\theta}{\partial\eta^{2}} + \operatorname{ScSr}\frac{\partial^{2}\theta}{\partial\eta^{2}} - \gamma\operatorname{Sc} \phi = 0$$
(12)

$$\frac{\partial f(\xi, 0)}{\partial \eta} = 1, \quad f(\xi, 0) = -\xi \frac{\partial f(\xi, 0)}{\partial \xi}, 
\frac{\partial \theta(\xi, 0)}{\partial \eta} = -\beta_1 (1 - \theta(0)) 
\frac{\partial \phi(\xi, 0)}{\partial \eta} = -\beta_2 (1 - \phi(0)) 
\frac{\partial f(\xi, \infty)}{\partial \eta} = 0, \quad \theta(\xi, \infty) = 0, \quad \phi(\xi, \infty) = 0$$
(13)

where  $\in_1$  denotes the variable viscosity parameter,  $\Pr = \frac{v_f}{a_f}$ the Prandtl number,  $Sc = \frac{v_f}{D_h}$  the Schmidt number,  $\operatorname{Ec} \left[ = \frac{u_0^2 l^2}{(c_0)_f (T_w - T_\infty)} \right] \quad \text{the Eckert number,} \quad M \left[ = \frac{\sigma_f B_0^2}{a \rho_f} \right]$ Hartmann number,  $\beta_t \left[ = \frac{g^* \beta^* (T_w - T_\infty)}{a^2 l} \right]$  the mixed convection variable,  $y \left[ = \frac{k_{\rm r}^2}{a} \right]$  the reaction variable,  ${\rm Sr} \left[ = \frac{D_{\rm b} k_{\rm T} (T_{\rm W} - T_{\infty})}{T_{\rm m} (C_{\rm W} - C_{\infty}) \, v_{\rm f}} \right]$  the Soret number,  $\beta_c = \frac{\beta^{**}(C_w - C_{\infty})}{\beta^{*}(T_w - T_{\infty})}$  the buoyancy ratio parameter,  $\in_2$  variable thermal conductivity parameter,  $\in_3$ variable mass diffusivity parameter,  $Nt = \frac{\tau D_T(T_w - T_{\infty})}{T_{\infty}V_f}$  thermophoresis variable,  $Nb \left| = \frac{\tau D_b(C_w - C_\infty)}{v_f} \right|$  Brownian motion variable,  $\operatorname{Du}\!\left(=\frac{D_b k_{\mathrm{T}}(C_{\mathrm{W}}-C_{\mathrm{co}})}{(c_{\mathrm{p}})_{\mathrm{f}}C_{\mathrm{s}}\nu_{\mathrm{f}}}\right)$  the Dufour number,  $\beta_1\!\!\left(=\frac{h_{\mathrm{f}}}{k_{\mathrm{f}}\sqrt{\frac{a}{\nu_{\mathrm{f}}}}}\right)$  thermal Biot number,  $\operatorname{Fr}\!\left(=\frac{C_{\mathrm{b}}}{\sqrt{k_{\mathrm{p}}}}l\right)$  Darcy-Forchheimer number,  $\operatorname{Br}(=\operatorname{PrEc})$  Brinkman number,  $\beta_2\!\!\left(=\frac{h_{\mathrm{w}}}{D_{\mathrm{b}}\sqrt{\frac{a}{\nu_{\mathrm{f}}}}}\right)$  solutal Biot number, and  $\lambda\!\!\left(=\frac{\nu_{\mathrm{f}}}{ak_{\mathrm{p}}}\right)$  porosity parameter.

# 3 Engineering quantities

# 3.1 Drag force coefficient

Mathematically,

$$C_{f,x} = \frac{\tau_{xy}}{\rho_{\rm f} u_{\rm w}^2},$$

Shear stress  $\tau_{xy}$  is

$$\tau_{xy} = \mu(T) \left( \frac{\partial u}{\partial y} \right) \bigg|_{y=0}$$
, (15)

Dimensionless form

$$C_{fx} \operatorname{Re}_{x}^{1/2} = (1 + \epsilon_{1} \theta(0)) f''(0).$$
 (16)

#### 3.2 Nusselt number

Mathematically, it is given as

$$Nu_x = \frac{xq_w}{k_f(T_w - T_\infty)},$$
(17)

Heat flux  $q_w$  satisfies

$$q_{\rm w} = -k(T) \left( \frac{\partial T}{\partial y} \right) \bigg|_{y=0}$$

(18)

Dimensionless form

$$\text{Nu}_x \text{Re}_x^{-1/2} = -(1 + \in_2 \theta(0))\theta'(0).$$

#### 3.3 Sherwood number

Mathematically,

$$Sh_{x} = \frac{xj_{w}|_{y=0}}{D_{b}(C_{w} - C_{\infty})},$$

The heat flux  $j_w$  is defined as

$$j_{\rm w} = -D_{\rm B}(C) \left( \frac{\partial C}{\partial y} \right), \tag{21}$$

The dimensionless form is

$$\operatorname{Sh}_{x} \operatorname{Re}_{x}^{-1/2} = -(1 + \in_{3} \phi(0)) \phi'(0).$$
 (22)

Here,  $Re_x = \frac{u_w x}{v}$ , indicates the local Reynolds number.

# 4 Solution development

## 4.1 First-order truncation

For the first-order truncation, we suppose that  $\frac{\partial(.)}{\partial \xi}(=0)$  and  $\frac{\partial(.)}{\partial \eta}(=')$  in Eqs. (10)–(13).

$$(1 + \epsilon_1 \theta) f''' + \epsilon_1 \theta' f'' + f f'' - f'^2 - M f' - \lambda f'$$

$$- \operatorname{Fr} \xi f'^2$$

$$+ \frac{\beta_t}{\xi} (\theta + \beta_c \phi) = 0$$
(23)

$$(1 + \epsilon_2 \theta)\theta'' + \epsilon_2 \theta'^2 + \Pr f \theta' + \Pr \text{Nb}\theta' \phi' + \Pr \text{Nt}\theta'^2 + M \text{Br} \xi^2 f'^2 + \Pr \text{Du}\phi'' = 0$$

$$(1 + \epsilon_3 \phi) \phi'' + \epsilon_3 {\phi'}^2 + \operatorname{Sc} f \phi' + \frac{Nt}{Nb} \theta'' + \operatorname{ScSr} \theta''$$
$$- y \operatorname{Sc} \phi = 0, \tag{25}$$

$$f'(\xi, 0) = 1, f(\xi, 0) = 0, \theta'(\xi, 0) = -\beta_1(1 - \theta(0))$$
  

$$\phi'(\xi, 0) = -\beta_2(1 - \phi(0))$$
  

$$f'(\xi, \infty) = 0, \theta(\xi, \infty) = 0, \phi(\xi, \infty) = 0$$
(26)

# 4.2 Second-order truncation

(19) For the second- order truncation, we suppose that  $\frac{\partial f}{\partial \xi} = p$ ,  $\frac{\partial^2 f}{\partial \xi \partial \eta} = \frac{\partial p}{\partial \eta}, \quad \frac{\partial^3 f}{\partial \xi \partial \eta^2} = \frac{\partial^2 p}{\partial \eta^2}, \quad \frac{\partial \theta}{\partial \xi} = q, \quad \frac{\partial^2 \theta}{\partial \xi \partial \eta} = \frac{\partial q}{\partial \eta}, \quad \frac{\partial \varphi}{\partial \xi} = g, \quad \text{and}$  $\frac{\partial^2 \varphi}{\partial \xi \partial \eta} = \frac{\partial g}{\partial \eta}, \text{ in Eqs. (10)-(13). We have}$ 

$$(1 + \epsilon_{1}\theta)\frac{\partial^{3}f}{\partial\eta^{3}} + \epsilon_{1}\frac{\partial\theta}{\partial\eta}\frac{\partial^{2}f}{\partial\eta^{2}} + f\frac{\partial^{2}f}{\partial\eta^{2}} + \xi p\frac{\partial^{2}f}{\partial\eta^{2}} - \left(\frac{\partial f}{\partial\eta}\right)^{2} - \left(\frac{\partial f}{\partial\eta}\right)^{2} - \xi\frac{\partial p}{\partial\eta}\frac{\partial f}{\partial\eta} - M\frac{\partial f}{\partial\eta} - \lambda\frac{\partial f}{\partial\eta} - \operatorname{Fr}\xi\left(\frac{\partial f}{\partial\eta}\right)^{2} + \frac{\beta_{t}}{\xi}(\theta + \beta_{c}\phi) = 0$$
(27)

$$(1 + \epsilon_{2}\theta)\frac{\partial^{2}\theta}{\partial\eta^{2}} + \epsilon_{2}\left[\frac{\partial\theta}{\partial\eta}\right]^{2} + \operatorname{Pr}\xi p\frac{\partial\theta}{\partial\eta} + \operatorname{Pr}f\frac{\partial\theta}{\partial\eta}\right]$$

$$-\operatorname{Pr}\xi q\frac{\partial f}{\partial\eta} + \operatorname{PrNb}\frac{\partial\theta}{\partial\eta}\frac{\partial\phi}{\partial\eta} + \operatorname{PrNt}\left[\frac{\partial\theta}{\partial\eta}\right]^{2}$$

$$+M\operatorname{Br}\xi^{2}\left[\frac{\partial f}{\partial\eta}\right]^{2} + \operatorname{PrDu}\frac{\partial^{2}\phi}{\partial\eta^{2}} = 0$$

$$(28)$$

$$(1 + \epsilon_{3}\phi)\frac{\partial^{2}\phi}{\partial\eta^{2}} + \epsilon_{3}\left(\frac{\partial\phi}{\partial\eta}\right)^{2} + \operatorname{Sc} f\frac{\partial\phi}{\partial\eta} + \operatorname{Sc}\xi p\frac{\partial\phi}{\partial\eta} - \operatorname{Sc}\xi g\frac{\partial f}{\partial\eta} + \frac{\operatorname{Nt}}{\operatorname{Nb}}\frac{\partial^{2}\theta}{\partial\eta^{2}} + \operatorname{ScSr}\frac{\partial^{2}\theta}{\partial\eta^{2}} - \gamma \operatorname{Sc}\phi = 0$$

$$(29)$$

$$\frac{\partial f(\xi, 0)}{\partial \eta} = 1, \ f(\xi, 0) = -\xi p, \ \frac{\partial \theta(\xi, 0)}{\partial \eta} = -\beta_1 (1 - \theta(0))$$

$$\frac{\partial \phi(\xi, 0)}{\partial \eta} = -\beta_2 (1 - \phi(0))$$

$$\frac{\partial f(\xi, \infty)}{\partial \eta} = 0, \ \theta(\xi, \infty) = 0, \ \phi(\xi, \infty) = 0$$

$$(30)$$

Now in Eqs. (27)–(30) derivative with respect to " $\xi$ " and the terms having  $\frac{\partial p}{\partial \xi}$ ,  $\frac{\partial^2 p}{\partial \xi \partial \eta}$ ,  $\frac{\partial^3 p}{\partial \xi \partial \eta^2}$ ,  $\frac{\partial q}{\partial \xi}$ ,  $\frac{\partial^2 q}{\partial \xi \partial \eta}$ ,  $\frac{\partial g}{\partial \xi}$ ,  $\frac{\partial^2 g}{\partial \xi \partial \eta}$  are vanished and  $\frac{\partial(\cdot)}{\partial n}$  denoting by prime.

$$(1 + \epsilon_{1}\theta)p''' + \epsilon_{1}qf''' + \epsilon_{1}q'f'' + \epsilon_{1}\theta'p'' + 2pf'' + fp'' + \xi pp'' - 3f'p' - \xi p'^{2} - Mp' - \lambda p' - Fr f'^{2} - 2Fr f'p' - \frac{\beta_{t}}{\xi^{2}}(\theta + \beta_{c}\phi) + \frac{\beta_{t}}{\xi}(q + \beta_{c}g) = 0$$
(31)

$$(1 + \epsilon_2 \theta)q'' + \epsilon_2 q \theta'' + 2 \epsilon_2 \theta' q' + 2 \operatorname{Pr} p \theta' + \operatorname{Pr} f q'$$

$$- \operatorname{Pr} q f' - \operatorname{Pr} \xi p' q + \operatorname{Pr} \xi p q'$$

$$+ \operatorname{Pr} \operatorname{Nb} \theta' g' + \operatorname{Pr} \operatorname{Nb} q' \phi' + 2 \operatorname{Pr} \operatorname{Nt} \theta' q' + 2 \operatorname{MBr} \xi f'^2$$

$$+ 2 \operatorname{MBr} \xi^2 f' p' + \operatorname{Pr} \operatorname{Du} g'' = 0$$

$$(32)$$

$$(1 + \epsilon_3 \phi)g'' + \epsilon_3 g \phi'' + 2 \epsilon_3 \phi' g' + \operatorname{Sc} p \phi' + \operatorname{Sc} f g'$$

$$- \operatorname{Sc} g f' - \operatorname{Sc} \xi p' g + \operatorname{Sc} \xi p g'$$

$$\frac{\operatorname{Nt}}{\operatorname{Nb}} q'' + \operatorname{Sc} \operatorname{Sr} q'' - y \operatorname{Sc} g = 0$$

$$(33)$$

$$p'(\xi, 0) = 0, \ p(\xi, 0) = 0, \ q'(\xi, 0) = \beta_1 q(\xi, 0)$$
 
$$g'(\xi, 0) = \beta_2 g(\xi, 0)$$
 
$$p'(\xi, \infty) = 0, \ q(\xi, \infty) = 0, \ g(\xi, \infty) = 0$$
 
$$(34)$$

#### 5 HAM

The assessment of problem is presented with the implementation of optimal HAM. HAM scheme is implemented in wide range to different nonlinear problems in era of engineering, biology, sciences, and industrial processes. The motivations for utilizing HAM technique preserve

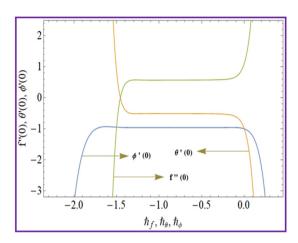


Figure 2:  $\hbar$ -curves.

less residual error. The excellent convergence criteria are associated with this method. Defining the initial guesses and linear operators as follows:

$$f_{0}(\eta) = 1 - e^{-\eta}$$

$$\theta_{0}(\eta) = \frac{\beta_{1}}{(1+\beta_{1})}e^{-\eta}$$

$$\phi_{0}(\eta) = \frac{\beta_{2}}{(1+\beta_{2})}e^{-\eta}$$
(35)

$$L_{\rm f} = \frac{\partial^3}{\partial \eta^3} - \frac{\partial}{\partial \eta}$$

$$L_{\theta} = \frac{\partial^2}{\partial \eta^2} - 1$$

$$L_{\phi} = \frac{\partial^2}{\partial \eta^2} - 1$$
(36)

subject to

$$L_{f}[c_{0} + c_{1}e^{-\eta} + c_{2}e^{\eta}] = 0, \quad L_{\theta}[c_{3}e^{-\eta} + c_{4}e^{\eta}] = 0,$$

$$L_{\phi}[c_{5}e^{-\eta} + c_{6}e^{\eta}] = 0$$
(37)

Here,  $c_i(i = 0, 1, 2, ..., 6)$  represents the arbitrary constants.

# 6 Convergence analysis

The auxiliary parameters  $\hbar_{\mathrm{f}}$ ,  $\hbar_{\theta}$ , and  $\hbar_{\phi}$  play a significant role in controlling the convergence of solutions. The  $\hbar$ -curves are shown in Figure 2. The ranges for meaningful values are  $-1.4 \le h_f \le -0.1$ ,  $-1.3h_\theta \le -0.3$ , and  $-1.3 \le h_\phi \le -0.2$ . Various orders of approximation for flow variables are highlighted in Table 1.

## 7 Validation of results

Table 2 has been meticulously crafted to provide a solid foundation for validating our current findings by

Table 1: Various order of approximation for various flow parameters

| Order of approximation | -f'' (0) | heta'  | φ′ (0) |
|------------------------|----------|--------|--------|
| 1                      | 1.172    | 0.9845 | 0.9845 |
| 8                      | 1.180    | 0.9119 | 0.9119 |
| 12                     | 1.180    | 0.8562 | 0.8354 |
| 18                     | 1.180    | 0.8562 | 0.8354 |
| 22                     | 1.180    | 0.8562 | 0.8354 |
| 24                     | 1.180    | 0.8409 | 0.8264 |
| 28                     | 1.180    | 0.8362 | 0.8153 |
| 30                     | 1.180    | 0.8362 | 0.8153 |

**Table 2:** Comparative analysis of heat transport rate with Khan et al. [39]

| Pr   | Khan <i>et al</i> . [40] | Recent results |
|------|--------------------------|----------------|
| 0.07 | 0.065609                 | 0.065612       |
| 0.20 | 0.169115                 | 0.169121       |
| 0.70 | 0.453920                 | 0.453931       |
| 2.00 | 0.911435                 | 0.911439       |

juxtaposing them with previously published results in the existing body of literature. In this analysis, we have focused on comparing the heat transport rate against higher estimations of the Prandtl number, while holding all other parameters constant, and we have specifically referenced the work of Khan *et al.* [39]. Remarkably, our results exhibit a remarkable concurrence with Wang's findings, strengthening the credibility of this study.

# 8 Analysis of results

Physical analysis for observing the profiles of velocity, concentration, and thermal distribution is interpreted. Graphical description of skin friction, solutal transport rate, and Nusselt number for secondary variables is explored.

## 8.1 Velocity profile

The phenomenon of velocity profile  $f'(\eta)$  via variable viscosity parameter  $\in_1$  is portrayed in Figure 3. An increment in velocity is detected *versus* higher variable viscosity parameter. The flow Hartmann constant M is sketched in Figure 4. An increment in resistive force is witnessed with variation in magnetic field, which leads to decays velocity. Such results are physically attributed to the role of Lorentz

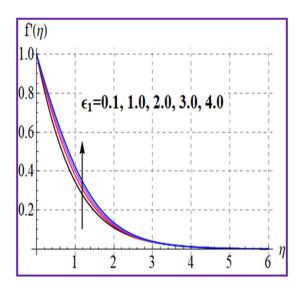


Figure 3:  $f'(\eta)$  vs  $\in_1$ .

force, which resists the fluid movement. The performance of  $f'(\eta)$  against porosity constant  $\lambda$  is illustrated in Figure 5. An enhancement in  $\lambda$  leads to upsurges viscous force and so fluid motion decays. Physically, this retarded behavior is due to the permeability of porous medium. The variation of Darcy–Forchheimer constant Fr on  $f'(\eta)$  is displayed in Figure 6. An enhancing function for velocity change due to Fr is claimed. Physical aspects for this change are the applications of inertial forces.

#### 8.2 Temperature profile

The feature of temperature profile  $\theta(\eta)$  *via* thermal Biot number  $\beta_1$  is shown in Figure 7. In fact, higher  $\beta_1$ 

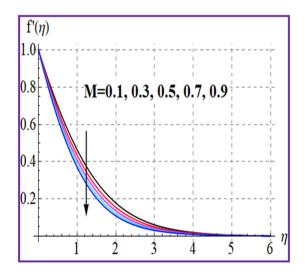


Figure 4:  $f'(\eta)$  vs M.

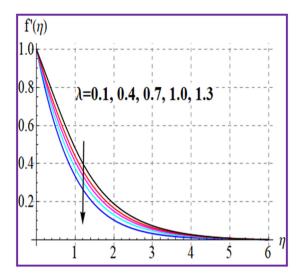
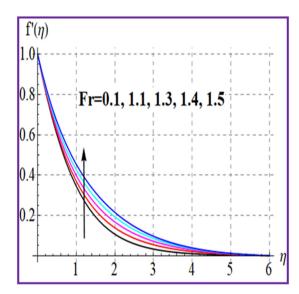


Figure 5:  $f'(\eta)$  vs  $\lambda$ .



**Figure 6:**  $f'(\eta)$  vs Fr.

corresponds to generate an additional heat in system that upgrades thermal field. The improvement in profile of  $\theta(\eta)$ is due to the fact that  $\beta_1$  is physically attributed to the enhancement in heat transfer coefficient. Figure 8 shows the impact of variable thermal conductivity parameter  $\in_2$ on  $\theta(\eta)$ . The assumptions of variable thermal conductivity are more effective to increase the heat transfer rate. The variation of thermophoresis parameter Nt and Brownian constant Nb on temperature is shown in Figures 9 and 10, respectively. Improvement in  $\theta(\eta)$  is observed due to both Nt and Nb. Physically, Nt involves the thermophoresis phenomenon, which leads to the movement of fluid liquids in cold surface. Such migration confirmed the improvement in heat transfer. Furthermore, increasing change in  $\theta(\eta)$ 

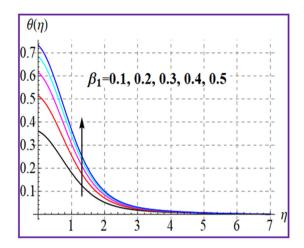


Figure 7:  $\theta(\eta)$  vs  $\beta_1$ .

regarding the variation of Nb involves the Brownian movement. In Figure 11, the temperature distribution  $\theta(\eta)$  is enhanced via the Brinkman number Br. Physically boosting in Br implies a lower distribution to the thermal conduction caused by viscous dissipation, which enlarges the temperature. Figure 12 depicts the magnification of  $\theta(\eta)$  against the Dufour number Du. Larger approximation of Dufour constant Du corresponds to intensify the thermal distribution. Physically, increasing change in Du leads to enhanced thermal diffusivity because  $\theta(\eta)$  gets boosted.

#### 8.3 Concentration profile

Figures 13 and 14 are sketched to show the fluctuation in  $\phi(\eta)$  against Nt and Nb. An improvement in  $\phi(\eta)$  is claimed for Nt, while the reverse change is addressed for Nb.

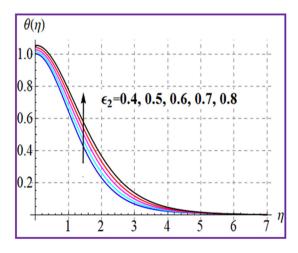
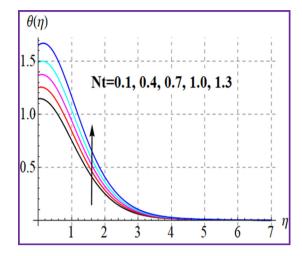
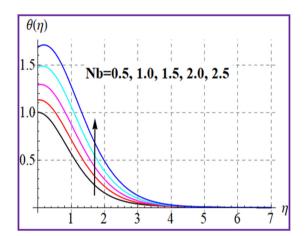


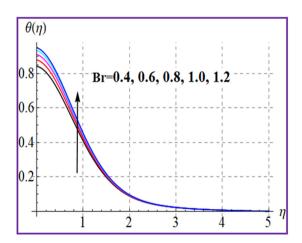
Figure 8:  $\theta(\eta)$  vs  $\in_2$ .



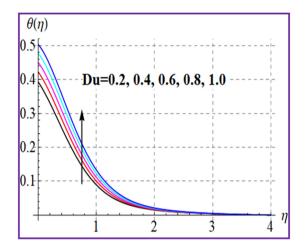
**Figure 9:**  $\theta(\eta)$  vs Nt.



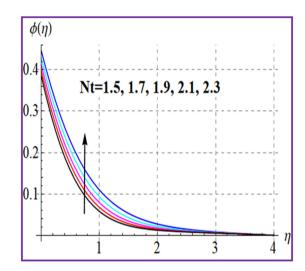
**Figure 10:**  $\theta(\eta)$  *vs* Nb.



**Figure 11:**  $\theta(\eta)$  *vs* Br.



**Figure 12:**  $\theta(\eta)$  vs Du.



**Figure 13:**  $\phi(\eta)$  *vs* Nt.

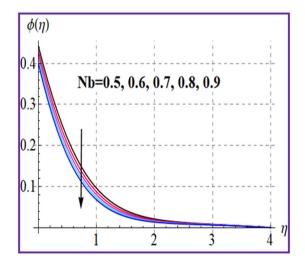


Figure 14:  $\phi(\eta)$  vs Nb.

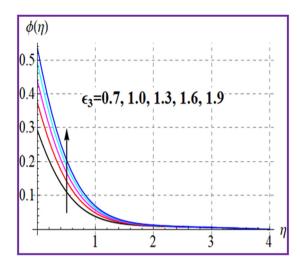


Figure 15:  $\phi(\eta)$  vs  $\in_3$ .

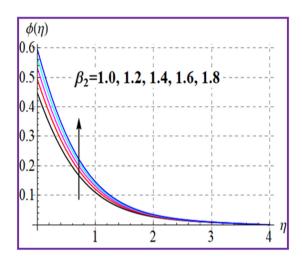
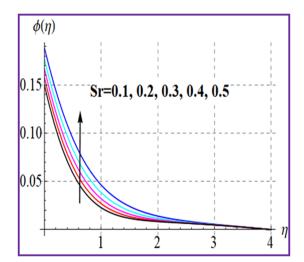


Figure 16:  $\phi(\eta)$  vs  $\beta_2$ .



**Figure 17:**  $\phi(\eta)$  vs Sr.

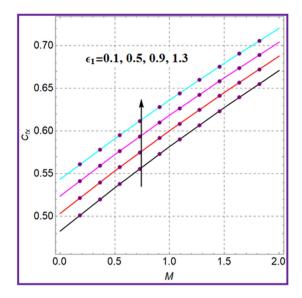


Figure 18:  $C_{fx}$  vs M and  $\in_1$ .

Improvement in  $\phi(\eta)$  is due to thermophoresis phenomenon. Figure 15 demonstrates the impact of variable mass diffusivity coefficient ∈3 on  $\phi(\eta)$ . An increment in ∈3 leads to an enlargement in  $\phi(\eta)$ . The influence of  $\beta_2$  on  $\phi(\eta)$  is illustrated in Figure 16. An improvement in concentration distribution via higher  $\beta_2$  is noted. Concentration trend for the found Soret Sr number is displayed in Figure 17. Clearly, larger values of Soret number Sr lead to enhancement in molar mass diffusivity. Consequently, concentration is increased.

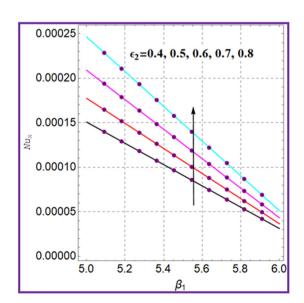


Figure 19:  $Nu_x \text{ } vs \beta_1 \text{ and } \in_2$ .

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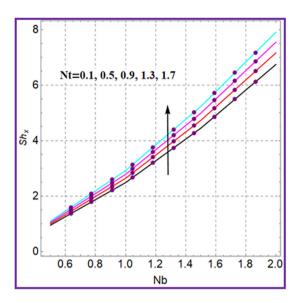


Figure 20:  $Sh_x$  vs Nt and Nb.

## 8.4 Physical quantities

Graphical description of drag force  $C_{fx}$ , solutal transport rate  $Sh_x$ , and Nusselt number  $Nu_x$  via secondary variables is interpreted in Figures 18–21. The influence of  $C_{fx}$  against M and variable viscosity  $\in_1$  variables is deployed in Figure 18. It is noted that drag force has an increasing trend for M and  $\in_1$ . Figure 19 is sketched to show the  $Nu_x$  variation versus the thermal Biot number  $\beta_1$  and variable conductivity factor  $\in_2$ . The heat transport rate has an increasing effect due to  $\beta_1$  and  $\in_2$ . The profile of Sherwood number  $Sh_x$  has a similar trend for the random variation of Nb and

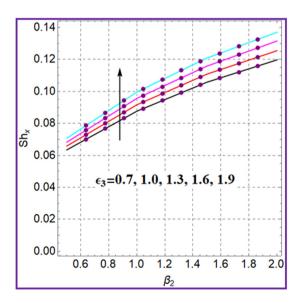


Figure 21:  $Sh_x vs \beta_2$  and  $\in_3$ .

thermophoresis constant Nt and visualized *via* Figure 20. Figure 21 claims that an increment in solutal transport rate is obtained for  $\beta_2$  and  $\epsilon_3$ .

# 9 Closing remarks

Mixed convective Darcy—Forchheimer flow of nanofluid is studied in the presence of viscous dissipation effects. The formulated problem is solved with optimal homotopy asymptotic method technique. Solution is validated with excellent accuracy. Major results are summarized as:

- An improvement in velocity profile is noted for Darcy– Forchheimer parameter and variable viscosity coefficient,
- The boosted change is observed in variable thermal conductivity parameter and the Brinkman number,
- With the Dufour number and the Biot constant, the heat transfer is sufficiently boosted,
- Larger solutal Biot number and variable mass diffusivity lead to an improvement in concentration field,
- The variation of wall shear force against the Hartmann number is enhanced for variable viscosity parameter,
- An increasing fluctuation of Sherwood number with the Brownian constant shows an increasing function with thermophoresis parameter,
- Such results can be further updated by incorporating the entropy generation phenomenon, artificial neural network, and sensitivity analysis.

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