

## Research Article

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# Effect of magnetic field and heat source on Upper-convected-maxwell fluid in a porous channel

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**Abstract:** The effect of magnetic field on the flow of the UCMF (Upper-Convected-Maxwell Fluid) with the property of a heat source/sink immersed in a porous medium is explored. A shrinking phenomenon along with the permeability of the wall are considered. The governing equations for the motion and transfer of heat of the UCMF along with boundary conditions are converted into a set of coupled nonlinear mathematical equations. Appropriate similarity transformations are used to convert the set of nonlinear partial differential equations into nonlinear ordinary differential equations. The modeled ordinary differential equations have been solved by the Homotopy Analysis Method (HAM). The convergence of the series solution is established. For the sake of comparison, numerical (ND-Solve method) solutions are also obtained. Special attention is given to how the non-dimensional physical parameters of interest affect the flow of the UCMF. It is observed that with the increasing Deborah number the velocity decreases and the temperature inside the fluid increases. The results show that the velocity and temperature distribution increases with a porous medium. It is also observed that the magnetic parameter has a decelerating effect on velocity while the temperature profiles increases in the entire domain. Due to the increase in Prandtl number the temperature profile increases. It is also observed that the heat source enhance the thermal conductivity and increases the fluid temperature while the heat sink provides a decrease in the fluid temperature.

**Keywords:** Heat source/sink, UCMF, Magnetohydrodynamic, Porosity, Shrinking channel

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## Nomenclature

$\beta$	Deborah number
$\eta$	Similarity variable
$\nu$	Kinematic viscosity ( $\text{m}^2\text{s}^{-1}$ )
$\theta$	Dimensionless temperature
$\varphi$	Stream function
$\lambda_1$	Internal heat generation/absorption parameter
$\lambda_R$	Relaxation time (t)
C	Dimensional constant ( $\text{t}^{-1}$ )
f	Similarity variable
K	Thermal conductivity
M	Magnetic field (Te)
$\text{Nu}_x$	Nusselt number
p	Density of the fluid ( $\text{kg m}^3$ )
Pr	Prandtl number
Q	Heat source/sink parameter
S	Suctions/injection parameter( $\text{ms}^{-1}$ )
T	Fluid's temperature (K)
$T_\infty$	Ambient temperature (K)
$T_w$	Wall temperature (K)
U, V	Velocity components ( $\text{ms}^{-1}$ )
$V_1, V_2$	Wall velocity
x,y	Cartesian coordinates (I)

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# 1 Introduction

The flow problem of a hydromagnetic fluid with the effects of porous media and heat transfer is one of the most important problems in the field of engineering and applied sciences. Recently, several mathematicians and applied researchers have proposed that the cooling rate be critical for products in order to improve their quality. For instance, the heat transfer is very important in extracting metal from ores. As a result, a number of field researchers from all of the developed countries recently studied various fluid mechanics problems in different flow configurations, including suction/blowing, magnetohydrodynamics, internal heat generation / absorption, rotation effects, permeability of the porous medium, simultaneous effects of energy and concentration process, viscous dissipations, Joule and Newtonian heating processes, etc. For example, hydromagnetic natural convection flow over a moving surface was studied by Fetecau *et al.* [1]. They presented the radiative heat transfer solution considering the effect of slip boundary conditions. Closed form solutions have been obtained by utilizing the Laplace transform and it was found that the slip parameter has significant effects on the solutions. A note on a Sisko fluid with radiation heat transfer was given by Mehmood and Fetecau [2]. Poiseuille flow was considered in an asymmetric channel and the effect of nonlinear wall temperature was investigated. The expressions for stream functions, axial velocities, and pressure were computed analytically. The micropolar fluid problem was studied by Sheikholeslami *et al.* [3] with heat transfer effects in a channel. The series solution was obtained by the homotopy perturbation method (HPM) and the effects of chemical reactions were investigated. Moreover, the effects of physical quantities such as Reynolds number, Peclet number, and micro rotation was analyzed and discussed through graphs. In another study, the same author [4] used the Differential Transform Method (DTM) for computations considering a micropolar fluid with high mass transfer filled in a porous channel. Ellahi *et al.* [5] analyzed the effects of heat transfer using third grade fluid in a channel. They obtained an analytical solution for axial velocity and temperature distribution for incompressible viscoelastic third grade fluid. Ellahi presented [6] the flow of nanofluid in a circular pipe. The effects of magnetohydrodynamic and variable viscosity are investigated in the solutions. MHD flow of a third grade fluid was investigated by Adesanya and Falade [7]. They explored the heat transfer rate of entropy in two parallel plates. The hydromagnetic slip flow over a shrinking wall of non-Newtonian fluid was computed by Turkyil-

mazoglu [8]. The dual and triple solutions were obtained. Raza *et al.* [9] presented the rotating flow of nanofluid with the effects of hydromagnetic and slip parameters. Freidoonimehr *et al.* [10] studied unsteady convective flow in a vertical permeable stretching surface with MHD effects. Rashidi *et al.* [11] used a permeable vertical sheet for the MHD free convective flow of non-Newtonian fluid. They presented the effects of radiation and buoyancy in their proposed model. The same author approached the similar procedure to study the mixed convective heat transfer for magnetohydrodynamic viscous fluid with thermal radiation and porous medium [12]. Rashidi *et al.* [13] gave an analytical solution for MHD viscoelastic fluid flow over a stretching surface with continuous motion. For this purpose they applied the homotopy analysis method (HAM). Zahid *et al.* [14] investigated the dual effects of viscous dissipation and thermal radiation on the stagnation point flow induced by an exponentially stretching wall. Awais *et al.* [15] studied the combined effects of Newtonian heating, thermal diffusion and diffusion thermos on an axisymmetric non-Newtonian fluid flow. In the present analysis, we have explored the solution for the internal heat generation/absorption phenomenon of the non-Newtonian Upper-convected-Maxwell fluid flow. The governing equations are first modeled and then solved analytically and numerically. In this context, the constitutive equations for velocity and temperature profiles are solved analytically by applying the homotopy analysis method (HAM).

This technique has already been used for the solution of various problems [16–37]. Ghadikolaei *et al.* [38] studied nonlinear thermal radiation effect on magneto Casson nanofluid flow with joule heating effect over an inclined porous stretching sheet. Hosseinzadeh *et al.* [39] investigated a numerical investigation on ethylene glycol-titanium dioxide nanofluid convective flow over a stretching sheet in presence of heat generation/absorption. Rahmati *et al.* [40] studied simultaneous investigations the effects of non-Newtonian nanofluid flow in different volume fractions of solid nanoparticles with slip and no-slip boundary conditions. Ghadikolaei *et al.* [41] carried out analytical and numerical solution of non-Newtonian second-grade fluid flow on a stretching sheet. Sheikholeslami *et al.* [42] studied heat transfer improvement and pressure drop during condensation of refrigerant-based nanofluid; an experimental procedure. Guo *et al.* [43] studied numerical study of nanofluids' thermal and hydraulic characteristics considering Brownian motion effect in a micro fin heat sink. Amini *et al.* [44] investigated thermal conductivity of highly porous metal foams using experimental and image based finite element analysis. Tian *et al.* [45] studied heat conduction investigation of functionally graded material

plates with variable gradient parameters under exponential heat source load [46–67].

Furthermore, for the sake of clarity the proposed method is also compared with ND-Solve method [68] and ADM [70, 71]. The effect of modeled parameters such as internal heat generation/absorption, porosity, magnetic parameter, suction/injection, and Deborah number on the solutions has been shown graphically and discussed. Furthermore, the present result was also compared with published work. A table has been constructed in order to represent the numerical values of a local Nusselt number of different involved physical quantities.

## 2 Statement of the problem

The system deals with two dimensional steady flow of an Upper-Convected-Maxwell fluid over a shrinking surface subject to a constant transverse magnetic field  $B_0$ . A porous channel is used to show the effects of suction/injection. The fluid saturates the porous medium for  $y > 0$  and the flow occupies the positive region  $y$ -axis. The porous medium saturates for  $y > 0$ . The shrinking velocity of the wall is  $V_1 = -Hw_1$  where and the suction/blowing parameter is represented by  $V_2$ . It is pointed out here that  $V_2 < 0$  represents suction phenomena while  $V_2 > 0$  corresponds to a blowing situation. It is also assumed that the temperature of the wall and free stream conditions are  $\theta_w$  and  $\theta_\infty$ , respectively. The heat generation or absorption  $q$  is also taken into account. In view of these assumptions, the governing basic flow equations are given in the following [1–5]:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0, \quad (1)$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + \lambda_R \left( u^2 \frac{\partial^2 u}{\partial x^2} + v^2 \frac{\partial^2 u}{\partial y^2} + 2uv \frac{\partial^2 u}{\partial x \partial y} \right) = v \frac{\partial^2 u}{\partial y^2} - \frac{\sigma B_0^2}{\rho_f} \left( u + \lambda_R v \frac{\partial u}{\partial y} \right) - \frac{v}{M_p} \left( u + \lambda_R v \frac{\partial u}{\partial y} \right), \quad (2)$$

$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \alpha \frac{\partial^2 T}{\partial y^2} + \frac{q}{\rho_f c_p} (T - T_\infty), \quad (3)$$

with the following boundary conditions

$$u = V_1, v = V_2, T = T_w \text{ at } y = 0, \quad (4)$$

$$u \rightarrow 0, T = T_\infty \text{ at } y \rightarrow \infty. \quad (5)$$

$u$  and  $v$  are the velocity components along the  $x$  and  $y$  axes, respectively. Here  $V_1 = -cx$  is the shrinking velocity of the

wall where  $c > 0$  and  $V_2$  is the suction/blowing. Furthermore,  $(x, y)$  represents the coordinate system,  $\lambda_R$  is relaxation time,  $\sigma$  is electrical conductivity,  $B_0$  is magnetic field strength,  $\rho_f$  is fluid density,  $M_p$  is permeability of porous media,  $T$  is fluid temperature,  $\alpha$  is thermal diffusivity, and  $c_p$  is the specific heat. Eqs. (2) and (3) can be transformed into a set of nonlinear ordinary differential equations by introducing the following similarity variables.  $u = \frac{\partial \phi}{\partial y}$ ,

$$u = \frac{\partial \phi}{\partial y}, v = \frac{\partial \phi}{\partial x}, \phi = (cv)^{1/2} x f(\eta), \eta = \sqrt{\frac{c}{v}}, \quad (6)$$

$$De = \lambda_R c, M^2 = \frac{\sigma B_0^2}{c \rho_f}, S = -V_2/(vc)^{1/2}, M_p = \frac{v}{c M_p},$$

$$\theta(\eta) = \frac{T - T_\infty}{T_w - T_\infty}, \alpha = \frac{k}{\rho_f c_p}, Pr = \frac{v}{\alpha}, \lambda_H = \frac{q}{c \rho_f c_p}.$$

The transformed ordinary differential equations are

$$f''' - (f')^2 + ff' + De (2ff'f'' - f^2f''') + M^2 De f f'' - M^2 f' - M_p f' + M_p De f f'' = 0, \quad (7)$$

$$\theta'' + Pr f \theta' + Pr \lambda_H \theta = 0. \quad (8)$$

The boundary conditions (4) and (5) become

$$f(0) = S, f'(0) = -1, f'(\infty) = 0, \quad (9)$$

$$\theta(0) = 1, \theta(\infty) = 0. \quad (10)$$

Here  $De = \lambda_R c$  represents the Deborah number in terms of relaxation time,  $M^2 = \frac{\sigma B_0^2}{c \rho_f}$  is the magnetic parameter,  $S = -V_2/(vc)^{1/2}$  is the suction/blowing parameter where  $S > 0$  means wall mass suction and  $S < 0$  means wall mass injection,  $M_p = \frac{v}{c M_p}$  is the porosity parameter,  $Pr = \frac{v}{\alpha}$  represents the Prandtl number,  $\lambda_H = \frac{q}{c \rho_f c_p}$  is the internal heat generation/absorption parameter, and prime represents differentiation with respect to  $\eta$ .

The local Nusselt number  $Nu_x$  is the physical quantity of interest for the readers. It is defined as

$$Nu_x = \frac{x q_w}{k(T_w - T_\infty)}, \quad (11)$$

where  $q_w$  (the wall heat flux) is defined as

$$q_w = -k \left( \frac{\partial T}{\partial y} \right)_{y=0}. \quad (12)$$

In dimensionless form we can write the above expression as

$$Nu_x / Re_x^{1/2} = -\theta'(0). \quad (13)$$

### 3 HAM solution

In order to solve Equations (7) and (8) under the boundary conditions (8) and (10), we utilize the homotopy analysis method (HAM) with the following procedure. The solutions having the auxiliary parameters  $\hbar$  regulate and control the convergence of the solutions. The initial guesses are selected as follows:

We select the initial approximation  $s$  such that the boundary conditions are satisfied as follows:

$$f_0(\eta) = s - 1 + e^{-\eta} \text{ and } \theta_0(\eta) = e^{-\eta}. \quad (14)$$

The linear operators are introduced as  $\mathfrak{S}_f$  and  $\mathfrak{S}_\theta$ :

$$\mathfrak{S}_f(f) = f' \text{ and } \mathfrak{S}_\theta(\theta) = \theta''. \quad (15)$$

With the following properties:

$$\mathfrak{S}_f(c_1 + c_2\eta + c_3\eta^2 + c_4e^{-\eta}) = 0 \text{ and } \mathfrak{S}_\theta(c_5 + c_6e^{-\eta}) = 0, \quad (16)$$

where  $c_i (i = 1 - 6)$  are arbitrary constants in general solution.

The nonlinear operators, according to (7) and (8), are defined as:

$$\begin{aligned} \mathfrak{N}_f[f(\eta; p)] &= \frac{\partial^3 f(\eta; p)}{\partial \eta^3} - \left( \frac{\partial f(\eta; p)}{\partial \eta} \right)^2 \\ &+ f(\eta; p) \frac{\partial f(\eta; p)}{\partial \eta} + De \left( 2f(\eta; p) \frac{\partial f(\eta; p)}{\partial \eta} \frac{\partial^2 f(\eta; p)}{\partial \eta^2} \right. \\ &\left. - (f(\eta; p))^2 \frac{\partial^3 f(\eta; p)}{\partial \eta^3} \right) + M^2 De \left( f(\eta; p) \frac{\partial^2 f(\eta; p)}{\partial \eta^2} \right) \\ &- (M^2 + M_p) \left( \frac{\partial f(\eta; p)}{\partial \eta} \right) + M_p De \left( f(\eta; p) \frac{\partial^2 f(\eta; p)}{\partial \eta^2} \right) \\ &= 0, \\ \mathfrak{N}_\theta[f(\eta; p), \theta(\eta; p)] &= \frac{\partial^2 \theta(\eta; p)}{\partial \eta^2} + Pr f \frac{\partial \theta(\eta; p)}{\partial \eta} \\ &+ Pr \lambda_H \theta(\eta; p). \end{aligned} \quad (17)$$

The auxiliary function becomes

$$H_f(\eta) = H_\theta(\eta) = e^{-\eta}. \quad (18)$$

The symbolic software Mathematica is employed to solve  $i$ th order deformation equations:

$$\begin{aligned} \mathfrak{S}_f[f_i(\eta) - \chi_i f_{i-1}(\eta)] &= \hbar_f \mathcal{H}_f[f(\eta)] R_{f,i}(\eta), \\ \mathfrak{S}_\theta[\theta_i(\eta) - \chi_i \theta_{i-1}(\eta)] &= \hbar_\theta \mathcal{H}_\theta(\eta) R_{\theta,i}, \end{aligned} \quad (19)$$

where  $\hbar$  is auxiliary non-zero parameter and

$$R_{f,i}(\eta) = f'''_{m-1} - \sum_{k=0}^{m-1} f'_{m-1-k} f'_k + \sum_{k=0}^{m-1} f_{m-1-k} f'_k \quad (20)$$

$$\begin{aligned} &+ 2De \left( \sum_{k=0}^{m-1} f_{m-1-k} \sum_{l=0}^k f'_{k-l} f''_l - \sum_{k=0}^{m-1} f_{m-1-k} \sum_{l=0}^k f'_{k-l} f'''_l \right) \\ &+ De \left( M^2 + M_p \right) \sum_{k=0}^{m-1} f'_{m-1-k} f''_k - \left( M^2 + M_p \right) f', R_{\theta,i}(\eta) \\ &= \theta''_{m-1} + Pr \sum_{k=0}^{m-1} f_{m-1-k} \theta'_k + Pr \lambda_H \theta_{m-1}, \end{aligned}$$

$$\chi_i = \begin{cases} 0, & \text{if } i \leq 1 \\ 1, & \text{if } i > 1, \end{cases}$$

are the involved parameters in HAM theory (for more information about the different steps of HAM see [16–24]).

To control and speed the convergence of the approximation series by the help of the so-called  $h$ -curve, it is significant to choose a proper value of auxiliary parameter. The calculation are carried out on a personal computer with 4GB RAM and 2.70GHz CPU. The  $h$ -curves of  $f(0)$  and  $\theta(0)$  obtained by the 18<sup>th</sup> order of HAM solution are shown in Figure 1 which take approximately less than a minute in the execution. To obtain the optimal values of auxiliary parameters, the averaged residual errors are defined as

$$\begin{aligned} Re_f &= \frac{d^3 f(\eta)}{\delta \eta^3} - \left( \frac{df(\eta)}{\delta \eta} \right)^2 + f(\eta) \frac{df(\eta)}{\delta \eta} \\ &+ De \left( 2f(\eta) \frac{df(\eta)}{d\eta} \frac{d^2 f(\eta)}{d\eta^2} - (f(\eta))^2 \frac{d^3 f(\eta)}{d\eta^3} \right) \\ &+ M^2 De \left( f(\eta) \frac{d^2 f(\eta)}{d\eta^2} \right) - (M^2 + M_p) \left( \frac{df(\eta)}{d\eta} \right) \\ &+ M_p De \left( f(\eta) \frac{d^2 f(\eta)}{d\eta^2} \right) = 0, \end{aligned} \quad (21)$$

$$Re_\theta = \frac{d^2 \theta(\eta)}{d\eta^2} + Pr f \frac{d\theta(\eta)}{d\eta} + Pr \lambda_H \theta(\eta). \quad (22)$$

In order to survey the accuracy of the present method, the residual errors for the 20<sup>th</sup> order of HAM solutions of (21) and (22) are illustrated in Figures 2 and 3, and listed numerically in Table 1. An efficient numerical (ND-Solve) method is also applied to solve the transformed equations (7) and (8) corresponding to the boundary conditions given in equations (9) and (10) and compared with a HAM solution graphically and numerically as shown in Figures 4-5 and Tables 1-2, respectively.

### 4 Results and discussion

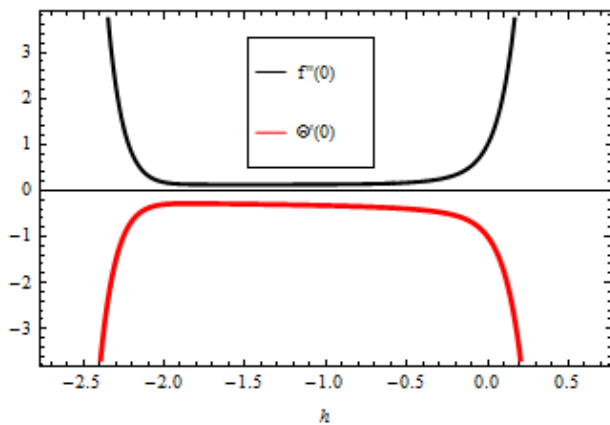
The transformed equations (7) and (8) subject to the boundary conditions (9) and (10) are solved analytically

**Table 1:** Numerical comparison of HAM and numerical method for  $f(\eta)$  when  $s = 1.5$ 

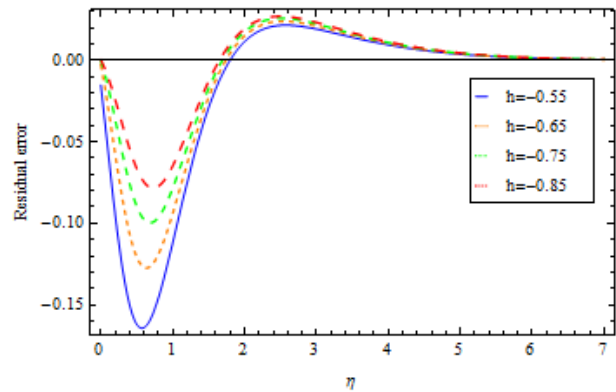
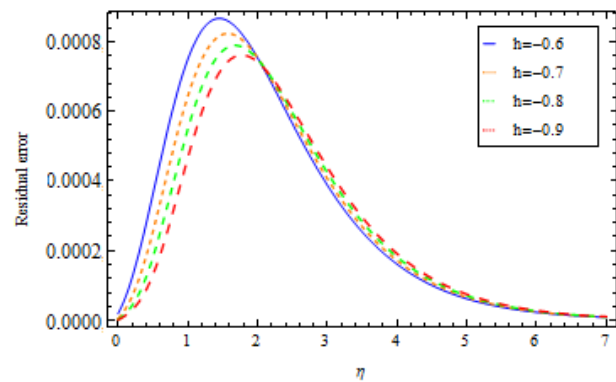
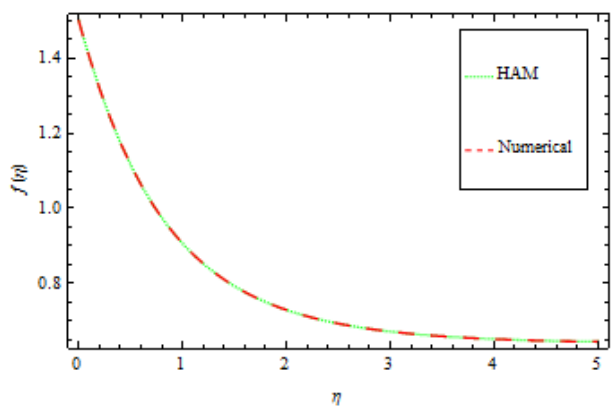
$\eta$	HAM	Numerical Solution	Absolute error
0	1.5	1.5	0
1	0.363339	0.295145	$0.2 \times 10^{-5}$
2	0.142604	0.054937	$0.7 \times 10^{-5}$
3	0.064857	0.014492	$0.5 \times 10^{-5}$
4	0.036777	0.033891	$0.8 \times 10^{-5}$
5	0.026519	0.037965	$0.4 \times 10^{-7}$
6	0.022756	0.033713	$0.3 \times 10^{-6}$
7	0.021372	0.01227	$0.5 \times 10^{-8}$

**Table 2:** Numerical comparison of HAM and numerical method for  $\theta(\eta)$  when  $s = 1$ ,  $De = M_p = \lambda_H = 0.1$ ,  $M = 0.2$ ,  $R = 0.3$  and  $Pr = 0.5$ 

$\eta$	HAM	Numerical Solution	Absolute error
0	1	1	0
1	0.394107	0.383863	$0.4 \times 10^{-6}$
2	0.147016	0.0968637	$0.1 \times 10^{-6}$
3	0.054222	0.018324	$0.1 \times 10^{-7}$
4	0.0199581	0.00242894	$0.3 \times 10^{-9}$
5	0.00734324	$5.14998 \times 10^{-9}$	$0.2 \times 10^{-11}$
6	0.00270155	-0.000160322	$0.3 \times 10^{-8}$
7	0.000993861	-0.0000814985	$0.1 \times 10^{-10}$

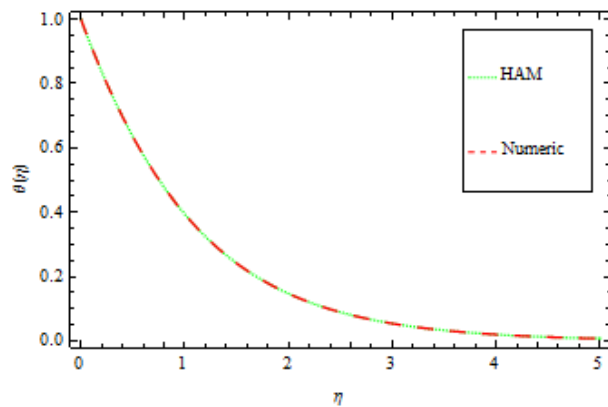
**Figure 1:** The  $h$ -curve of  $f(0)$  and  $\theta(0)$  obtained by the 18<sup>th</sup> order of HAM solution when  $De = M_p = \lambda_H = 0.1$ ,  $M = 0.2$ ,  $R = 0.3$  and  $Pr = 0.5$ 

by the homotopy analysis method. An efficient numerical method called ND-Solve method is also used for the sake of comparison. In this section, numerical values are assigned to the physical parameters involved in the velocity, tem-

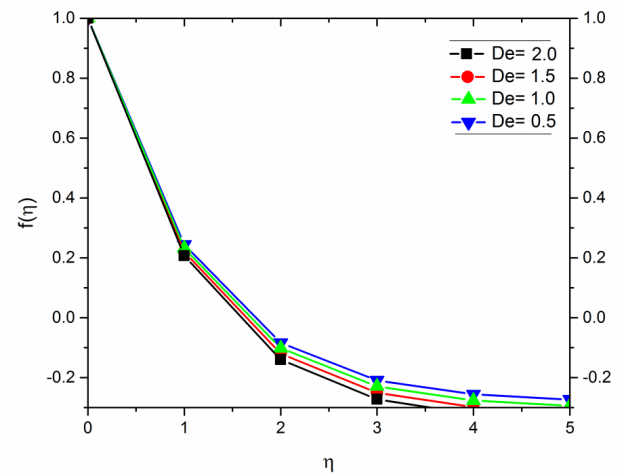
**Figure 2:** Residual error of Eq. (21) when  $De = M_p = \lambda_H = 0.1$ ,  $M = 0.2$ ,  $R = 0.3$  and  $Pr = 0.5$ **Figure 3:** Residual error of Eq. (22) when  $De = M_p = \lambda_H = 0.1$ ,  $M = 0.2$ ,  $R = 0.3$  and  $Pr = 0.5$ **Figure 4:** Comparison between HAM and Numerical solutions for velocity profile  $f(\eta)$  when  $s = 1.5$ ,  $De = M_p = 0.1$ ,  $\lambda_H = 0.2$ ,  $M = 0.2$  and  $R = 0.3$ 

perature and local Nusselt number. The paper examined the effects of governing parameters on the transient velocity profile, temperature profile and local Nusselt number. For this purpose the SRM approach has been applied for





**Figure 5:** Comparison between HAM and Numerical solutions for temperature profile  $\theta(\eta)$  when  $s = 1$ ,  $De = M_p = 0.1$ ,  $\lambda_H = 0.2$ ,  $M = 0.2$ ,  $R = 0.3$  and  $Pr = 0.5$



**Figure 6:** Effect of  $De$  on velocity profile  $f$  when  $S = 1$ ,  $M_p = 0.3$ ,  $M = 0.1$

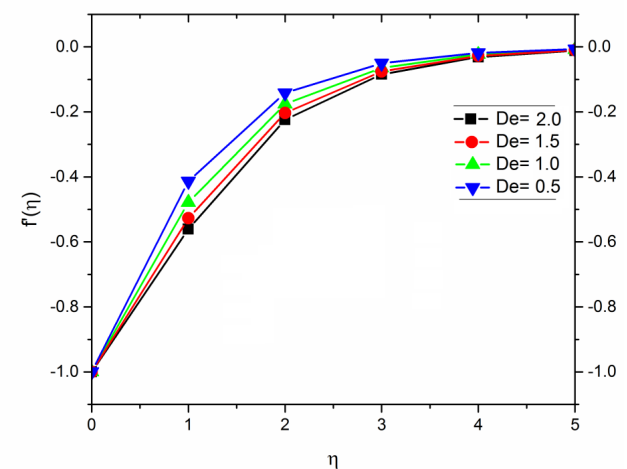
various values of flow controlling parameters  $De = 0.1$ ,  $M_p = 0.3$ ,  $\lambda_H = 0.2$ ,  $M = 0.2$ ,  $R = 0.3$  and  $Pr = 0.5$ , to obtain a clear insight into the physics of the problem. Therefore, all the graphs and tables correspond to the values above and the rest will be mentioned.

Figures 6 and 7 show the influence of Deborah number  $De$  on the velocities  $f$  and  $f'$  respectively. It is obvious from these figures that the boundary layer thickness decreases for larger values of  $De$ , with an increase in  $\eta$ . Physically, viscous effects increase for the larger Deborah numbers. These retard the flow in the entire domain and consequently the momentum boundary layer will be thinner. Since the Deborah number defines the difference between the solids and liquid (or fluids), the material shows fluid like behavior for a small Deborah number and for larger values of Deborah number the material behaves like a viscoelastic solid such as rubber, jelly, polymers etc. From the present analysis it is quite obvious that the velocity field decelerating for larger numbers.

Figure 8 and 9 depict the effects of porosity parameter  $M_p$  on  $f$  and  $f'$  respectively. It is observed that the velocity profile increases with increasing porosity parameter. Small variation is observed for  $f'$ . Furthermore, under the influence of constant magnetic field  $M = 0.3$ , the momentum boundary layer decreases due to the Lorentz force.

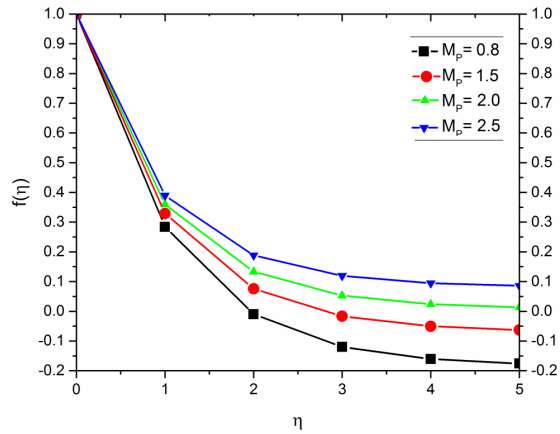
Figures 10 and 11 present the effects of suction/injection parameter  $s$  on  $f$  and  $f'$ . It is noticed that the velocity fields  $f$  and  $f'$  satisfy the far field boundary conditions (9) asymptotically, thus verifying the analytical and numerical results obtained.

Figure 12 displays the influence of magnetic field on the velocity profiles  $f$  with  $s = 1$ ,  $De = 0.1$ ,  $M_p = 0.3$ ,  $M = 0.2$  and  $R = 0.3$ . Due to the inflection of the vertical magnetic field to the electrically conducting fluid, the

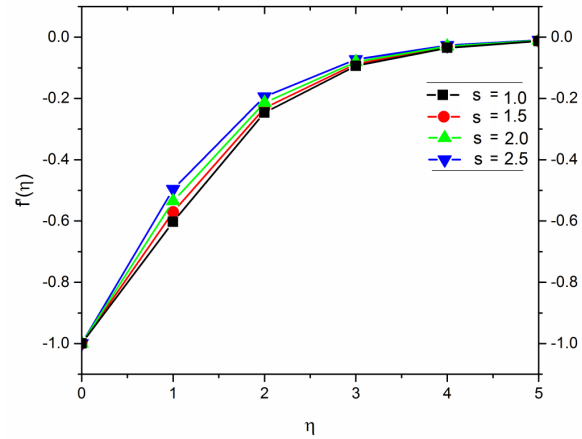


**Figure 7:** Effect of  $De$  on velocity profile  $f'$  when  $S = 1$ ,  $M_p = 0.3$ ,  $M = 0.1$

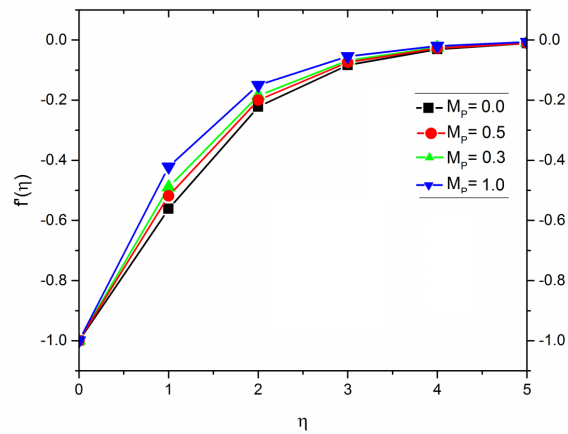
Lorentz force is produced. This force has the tendency to slow down the flow and as a result the velocity profile decreases. Figures 13-?? show the effect of different parameters on the temperature profiles. The effect of Prandtl number on the temperature distribution is shown in Figure 13. Based on the Prandtl number's definition  $Pr = \frac{\nu}{\alpha}$ , this parameter is defined as the ratio between the momentum diffusion to thermal diffusion. Thus, with the increase of Prandtl number the thermal diffusion decreases and so the thermal boundary layer becomes thinner as seen in Figure 13. It physically means that the flow with a large Prandtl number dissipates the heat faster to the fluid as the temperature gradient gets steeper and hence increases the heat transfer coefficient between the surface and the fluid. Figure 14 depicts the variation of Deborah number on the



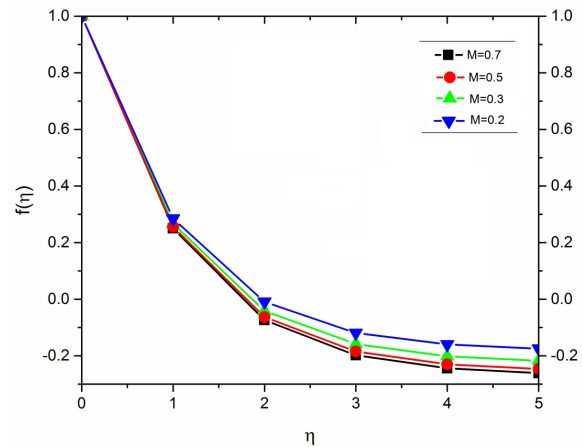
**Figure 8:** Effect of  $M_p$  on velocity profile  $f$  when  $S = 1$ ,  $De = 0.5$ ,  $M = 0.1$



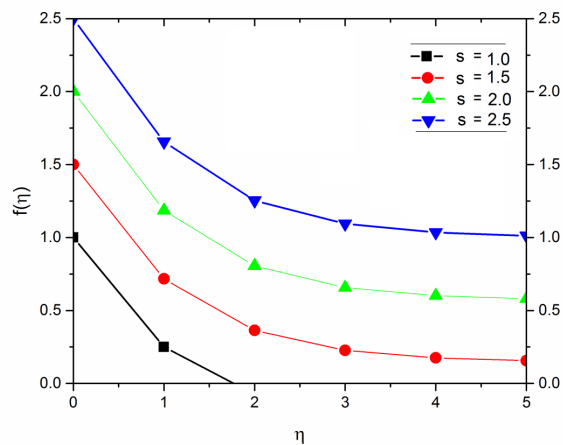
**Figure 11:** Effect of  $S$  on velocity profile  $f'$  when  $M_p = 0.2$ ,  $De = 0.5$ ,  $M = 0.1$



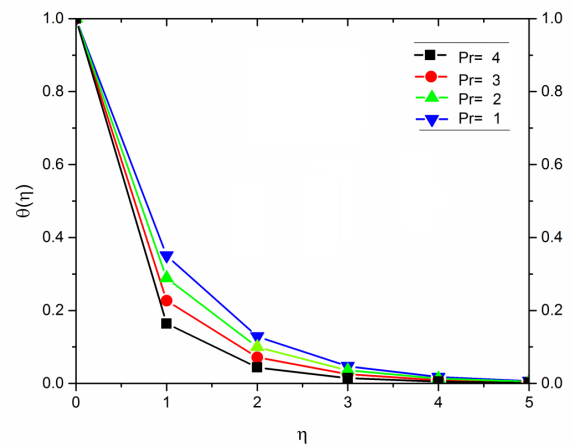
**Figure 9:** Effect of  $M_p$  on velocity profile  $f'$  when  $S = 1$ ,  $De = 0.5$ ,  $M = 0.1$



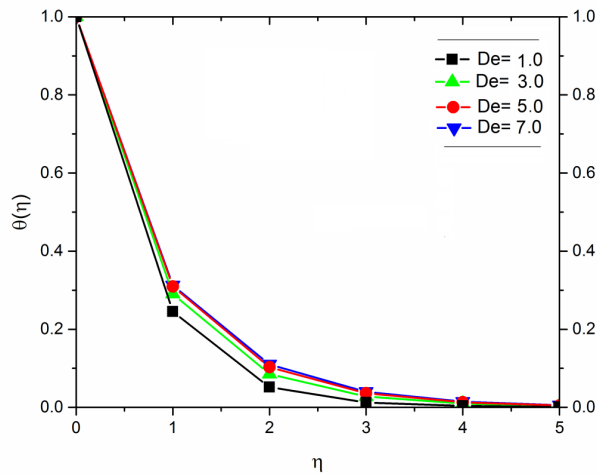
**Figure 12:** Effect of  $M$  on velocity profile  $f$  when  $M_p = 0.2$ ,  $De = 0.5$ ,  $S = 1$



**Figure 10:** Effect of  $S$  on velocity profile  $f$  when  $M_p = 0.2$ ,  $De = 0.5$ ,  $M = 0.1$



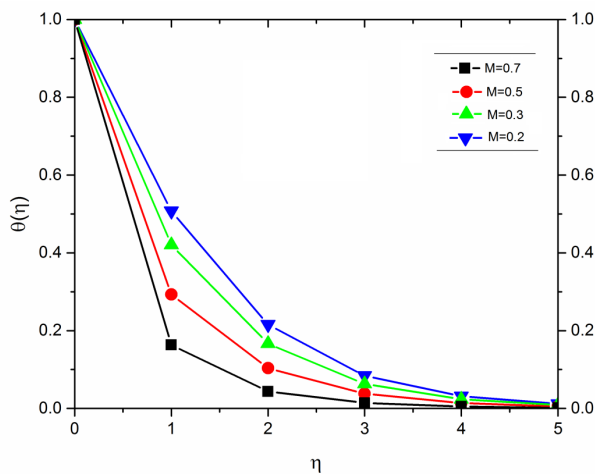
**Figure 13:** Effect of  $Pr$  on temperature profile  $\theta$  when  $M_p = 0.2$ ,  $De = 0.5$ ,  $S = 2$ ,  $M = 0.3$ ,  $\lambda_H = 0.2$



**Figure 14:** Effect of  $De$  on temperature profile  $\theta$  when  $M_p = 0.2$ ,  $S = 2$ ,  $Pr = 0.5$ ,  $M = 0.3$ ,  $\lambda_H = 0.2$

temperature distribution. Increasing the Deborah number  $De$  increases the temperature inside the fluid. Also, it is observed that for larger values of Deborah number the boundary layer thickness decreases with increasing  $\eta$ .

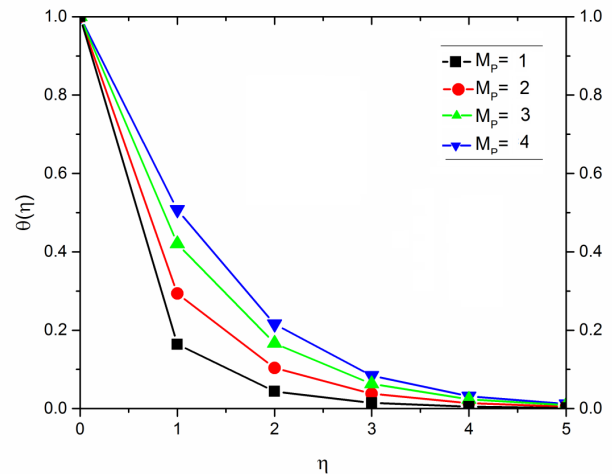
The influence of magnetic parameter  $M$  on the temperature distribution is shown in Figure 15. It is observed that the temperature distribution increases with increasing values of magnetic parameter  $M$ . Physically, the Lorentz force due to the transverse magnetic field has the property of relaxing the fluid velocity and temperature distributions. Accordingly, the velocity and temperature boundary layer thickness decreases as the magnetic parameter increases.



**Figure 15:** Effect of  $M$  on temperature profile  $\theta$  when  $M_p = 0.2$ ,  $S = 2$ ,  $Pr = 0.5$ ,  $De = 0.2$ ,  $\lambda_H = 0.2$

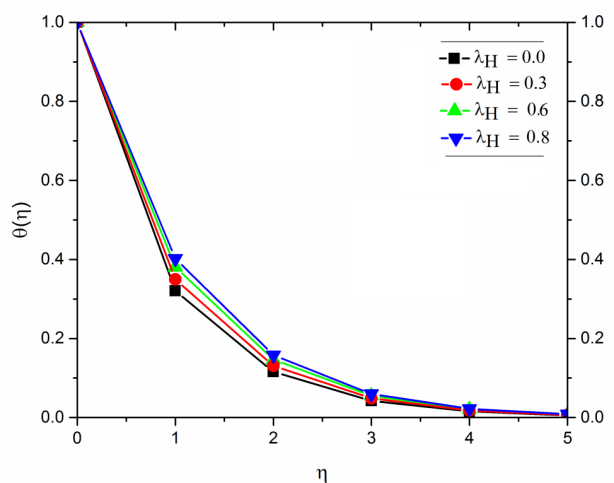
The effect of the porous permeability parameter  $M_p$  on the fluid temperature distribution is shown in Figure 16.

The result shows that as the porous permeability parameter increases, there is a corresponding increase in the fluid temperature due to increased diffusion of heat within the flow channel.



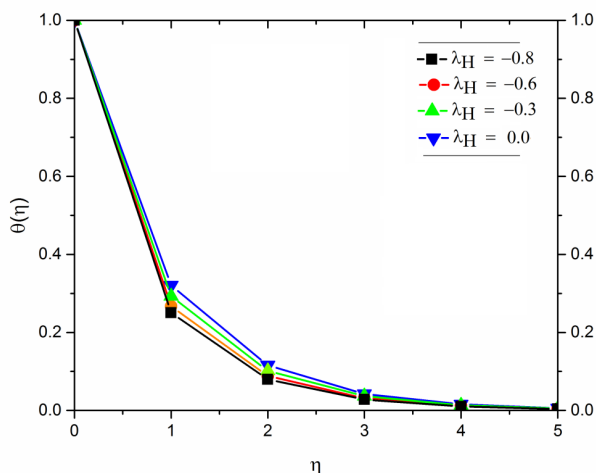
**Figure 16:** Effect of  $M_p$  on temperature profile  $\theta$  when  $M = 0.1$ ,  $S = 2$ ,  $Pr = 0.5$ ,  $De = 0.2$ ,  $\lambda_H = 0.2$

The effect of heat source ( $\lambda_H > 0$ ) and heat sink ( $\lambda_H < 0$ ) parameters are shown in Figures 17 and 18 respectively. It is observed that a heat source enhances the thermal conductivity and increases the fluid temperature as shown in Figure 13. Figure 14 incorporates the effects of the heat sink parameter. As expected, a heat sink provides a decrease in the fluid temperature.



**Figure 17:** Effect of heat generation  $\lambda_H > 0$  on temperature profile  $\theta$  when  $M = 0.1$ ,  $S = 2$ ,  $Pr = 0.5$ ,  $De = 0.2$





**Figure 18:** Effect of heat absorption  $\lambda_H < 0$  on temperature profile  $\theta$  when  $M = 0.1$ ,  $S = 2$ ,  $Pr = 0.5$ ,  $De = 0.2$

Table 3 shows different values of skin friction parameter  $-f^{(0)}$  for several values of permeability parameter  $M_p$ . We see from this table that the magnitude of shear stress in the boundary is smaller for injection in comparison to the case of suction. These results are in accordance with the physical situation because the injection of the fluid amounts to an increase of fluid velocity, resulting in a decrease of the frictional force. The permeability parameter introduces additional shear stress on the boundary. Note that the increase of permeability parameter leads to the increase of skin friction parameter in all the cases of suction, blowing, and impermeability of the surface.

**Table 3:** Values of skin friction parameter  $-f^{(0)}$  for several values of permeability parameter  $M_p$  when  $De = 0.1$ ,  $M = 0.2$

$s$	$M_p$	$-f^{(0)}$
1.2	0	3
	1	3.56785
	2	4.825621
0	0	2
	1	2.05710
	2	2.402051
-1.5	0	1.7
	1	1.801261
	2	1.913583

In order to discuss the results of local Nusselt number against different physical quantities including Deborah number, Prandtl number, and internal heat generation/absorption quantity, we have prepared Table 4. It is evident from this table that the local Nusselt number

decreases due to an increase in Deborah number and quantity of internal heat generation/absorption, whereas the local Nusselt number increases due to an increase in Prandtl number.

**Table 4:** Effect of various physical quantities on local Nusselt number  $-\theta'(0)$  including Deborah number, Prandtl number  $Pr$  and internal heat generation/absorption parameter  $\lambda_H$

$De$	$Pr$	$\lambda_H$	$-\theta'(0)$
0.0	1.0	0.2	2
0.1			1.283923
0.2			1.329046
0.1	0.1		0.163950
			1.320615
			2.325102
	0.1	-0.3	2.031823
		-0.1	1.325165
		0.2	2.290552
		0.4	1.221048

## 5 Conclusion

In this research paper, the semi-analytical/numerical technique known as HAM has been implemented to solve the transformed nonlinear differential equations describing the MHD flow of an Upper-Convected-Maxwell fluid with the influence of the internal heat generation/absorption. The dynamics of the magneto-hydrodynamic fluid flow in porous medium over a porous wall are investigated. The present semi-numerical/analytical simulations agree closely with the previous studies for some special cases. HAM has been shown to be a very strong and efficient technique in finding analytical solutions for nonlinear differential equations. HAM is shown to illustrate excellent convergence and accuracy and is currently being employed to extend the present study to mixed convective heat transfer simulations. The convergence of the series solution is established. Furthermore, the present method is also compared with an efficient numerical technique so called ND-Solve method. The effects of different physical key parameters which effect fluid motion such as Deborah number, magnetic parameter, suction/injection parameter, heat generation/absorption parameter, and porosity parameter are plotted and discussed. It is observed that with the increasing Deborah number the velocity decreases and the temperature inside the fluid increases. The

results show that the velocity and temperature distribution increases with a porous medium. It is also investigated that the magnetic parameter has a decelerating effect on velocity while the temperature profiles increases in the entire domain. Due to increase in Prandtl number the temperature profile increases. It is observed that the heat source enhance the thermal conductivity and increases the fluid temperature while the heat sink provides a decrease in the temperature fluids.

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