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Phase Transition and Thermal Expansion of $\text{Ba}_3\text{RB}_3\text{O}_9$ ($R = \text{Sm–Yb}$, and Y)

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Abstract: High temperature powder X-ray diffraction measurements of $\text{Ba}_3\text{RB}_3\text{O}_9$ ($R = \text{Sm–Yb}$, and Y) were carried out at temperatures ranging from room temperature to just below the corresponding melting temperatures (1,200–1,300 °C). No phase transition was found for the H-type phase ($R\bar{3}$) with $R = \text{Sm–Tb}$ and the L-type phase ($P6_3\text{ cm}$) with $R = \text{Tm–Yb}$. On the other hand, phase transition from the L phase to the H phase was observed for $R = \text{Dy–Er}$, and Y at around 1,100–1,200 °C. The obtained axial thermal expansion coefficient (ATEC) of the a -axis was larger than that of the c -axis for the H phase, and the ATEC of the c -axis was larger than that of the a -axis for the L phase. The observed anisotropic nature of ATEC is attributed to the distribution of the BO_3 anionic group with rigid boron–oxygen bonding in the structures of the H and L phases.

Keywords: borates, phase transition, thermal expansion, X-ray diffraction, high temperature

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Introduction

The $\text{Ba}_3\text{RB}_3\text{O}_9$ ($R = \text{rare earth element; REE}$) systems show two polymorphs corresponding to the type of REE. One is the H-type structure with the space group $R\bar{3}$ in the case of lighter REEs ($R = \text{Nd–Dy}$) (Figure 1(a)), and the other is the L-type structure with the space group $P6_3\text{ cm}$ reported for heavier REEs ($R = \text{Dy–Lu}$, and Y) (Figure 1(b)) [1–5]. The H-type structure of $\text{Ba}_3\text{RB}_3\text{O}_9$ is a potential host material for non-linear optical, laser, and scintillator application [6–10]. In particular, H-type compounds with Gd, Lu, or Y as the REE attract much interest as a potential host crystal in optical applications, because the

elements generally produce no unfavorable photoluminescence. In addition to the structural variation associated with the REE, the phase transition as a function of temperature was reported in systems with the middle rare earth elements and Y. For the practical use of the H-type structure, knowledge of the detailed conditions of chemistry and temperature for the phase stability in the $\text{Ba}_3\text{RB}_3\text{O}_9$ systems, and the corresponding physical properties such as the thermal expansion coefficient, is strongly required. This prompted us to conduct a systematic study of $\text{Ba}_3\text{RB}_3\text{O}_9$ compounds ($R = \text{Sm–By}$, and Y) with respect to their structure and high temperature behaviors. High temperature X-ray diffraction measurements were performed to confirm the crystal structural change and to clarify the axial thermal expansion coefficients (ATECs) of the H and L phases in the $\text{Ba}_3\text{RB}_3\text{O}_9$ systems ($R = \text{Sm–Yb}$, and Y).

Experimental

Sample preparation

Sample powders of $\text{Ba}_3\text{RB}_3\text{O}_9$ compounds ($R = \text{Sm–Yb}$, and Y) were prepared by the high-temperature solid-state reaction. Stoichiometric mixtures of raw chemicals ($4\text{N R}_2\text{O}_3$, 3N BaCO_3 , and $3\text{N H}_3\text{BO}_3$) were ground together and subsequently molded into pellets. Then, they were placed in alumina crucibles and sintered for 24 h at 1,000 °C in a muffle furnace. After the furnace was cooled down to room temperature (RT; 27 °C), the sintered pellets were crushed into powders for the following measurements.

Thermal analysis

Thermogravimetry-differential thermal analyses (TG-DTA) were performed for the prepared sample powders from RT to 1,350 °C using Pt pans with a Rigaku TG8120. Heating and cooling rates were 20 K/min. The obtained melting temperature was used for determining the temperature range for the high temperature powder X-ray diffraction (HT-XRD) measurements.

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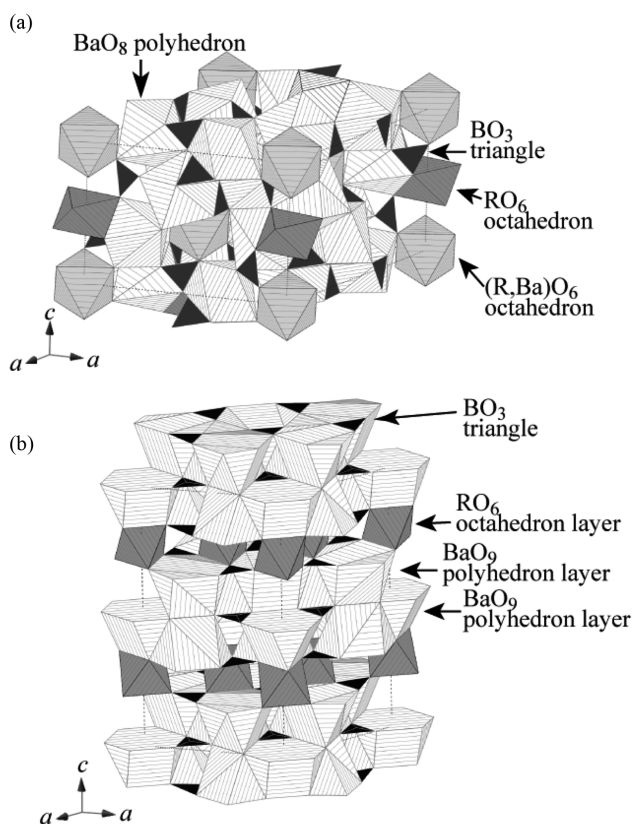


Figure 1: Schematic illustration of the crystal structures of the (a) H phase and (b) L phase. Oxygen-coordinated polyhedrons of cations ($R = \text{REE}$, Ba, and B) are drawn. The H phase is constructed of BO_3 triangles, BaO_8 polyhedrons, $(\text{Ba}, R)\text{O}_6$ octahedrons, and RO_6 octahedrons. The L phase is composed of three types of alternating layers; BO_3 triangles, BaO_9 polyhedrons, and RO_6 octahedrons.

X-ray diffraction measurements

The HT-XRD measurements utilized the ordinary Bragg-Brentano optics, a diffracted-beam monochromator, and Cu $K\alpha$ radiation. An electric furnace with a water-cooling device was placed at the center of a two-axes goniometer (Ultima III, Rigaku), and the temperature of the furnace was controlled using a R-type thermocouple. The temperature at the sample was calibrated using the result of high temperature X-ray diffraction for Al_2O_3 powder and the published standard data [11]. Temperatures of HT-XRD measurements during the heating period were set at RT, 200 °C, 400 °C, 600 °C, 800 °C, and 1,000 °C. In particular, intervals of 50 °C or 100 °C were also selected from 1,000 °C to the melting temperatures. For the cooling-down period over 800 °C, the HT-XRD measurements were performed at similar temperatures. In order to stabilize the temperature at the sample, HT-XRD measurements were started 5 min after reaching the target temperature. In our HT-XRD measurements, the

heating rate was set at 10 K/min below 1,000 °C and 5 K/min above 1,000 °C, and the cooling rate was set at 20 K/min.

Unit cell parameters were calculated by the least-square refinement with the computer program JADE ver. 6.5. The variations of the obtained unit cell parameters were analyzed using a quadratic function ($L = L_0 + L_1T + L_2T^2$, where L = the values of a or c axis, T = temperature (°C), and L_0 , L_1 , and L_2 are coefficients). The obtained coefficients are summarized in Table 1. ATEC ($\alpha_T = 1/L_0$

Table 1: The fitted coefficients for the quadratic curve shown in Figure 5 ($L = L_0 + L_1T + L_2T^2$).

R	a-axis		c-axis		
	Value	σ	Value	σ	
L phase					
Dy	L_0	9.426×10^0	2×10^{-3}	1.7642×10^1	9×10^{-3}
	L_1	9.0×10^{-5}	8×10^{-6}	1.7×10^{-4}	4×10^{-5}
	L_2	-2.2×10^{-8}	7×10^{-9}	2.2×10^{-7}	3×10^{-8}
Er	L_0	9.431×10^0	2×10^{-3}	1.7580×10^1	1×10^{-2}
	L_1	8.0×10^{-5}	8×10^{-6}	1.2×10^{-4}	6×10^{-5}
	L_2	-1.6×10^{-8}	6×10^{-9}	3.0×10^{-7}	5×10^{-8}
Ho	L_0	9.434×10^0	2×10^{-3}	1.7613×10^1	8×10^{-3}
	L_1	9.3×10^{-5}	7×10^{-6}	2.1×10^{-4}	3×10^{-5}
	L_2	-2.6×10^{-8}	6×10^{-9}	2.1×10^{-7}	2×10^{-8}
Tm	L_0	9.409×10^0	2×10^{-3}	1.7478×10^1	8×10^{-3}
	L_1	5.8×10^{-5}	7×10^{-6}	2.2×10^{-4}	3×10^{-5}
	L_2	— ^a	— ^a	2.2×10^{-7}	2×10^{-8}
Y	L_0	9.430×10^0	1×10^{-3}	1.7609×10^1	3×10^{-3}
	L_1	7.6×10^{-5}	4×10^{-6}	1.7×10^{-4}	1×10^{-5}
	L_2	-1.2×10^{-8}	3×10^{-9}	2.36×10^{-7}	8×10^{-9}
Yb	L_0	9.400×10^0	2×10^{-3}	1.7470×10^1	5×10^{-3}
	L_1	6.3×10^{-5}	9×10^{-6}	1.8×10^{-4}	2×10^{-5}
	L_2	— ^a	— ^a	2.4×10^{-7}	2×10^{-8}
H phase					
Dy	L_0	1.3049×10^1	4×10^{-3}	9.536×10^0	2×10^{-3}
	L_1	1.4×10^{-4}	2×10^{-5}	8.8×10^{-5}	8×10^{-6}
	L_2	1.2×10^{-7}	2×10^{-8}	-7.8×10^{-8}	7×10^{-9}
Eu	L_0	1.3079×10^1	8×10^{-3}	9.570×10^0	4×10^{-3}
	L_1	1.9×10^{-4}	3×10^{-5}	8.0×10^{-5}	2×10^{-5}
	L_2	1.0×10^{-7}	2×10^{-8}	-6×10^{-8}	1×10^{-8}
Gd	L_0	1.3078×10^1	2×10^{-3}	9.576×10^0	3×10^{-3}
	L_1	1.9×10^{-4}	1×10^{-5}	4×10^{-5}	1×10^{-5}
	L_2	1.0×10^{-7}	8×10^{-9}	-4×10^{-8}	1×10^{-8}
Ho	L_0	1.3061×10^1	2×10^{-3}	9.5451×10^0	7×10^{-4}
	L_1	1.4×10^{-4}	1×10^{-5}	9.2×10^{-5}	3×10^{-6}
	L_2	1.3×10^{-7}	8×10^{-9}	-8.5×10^{-8}	3×10^{-9}
Sm	L_0	1.3095×10^1	6×10^{-3}	9.576×10^0	4×10^{-3}
	L_1	1.9×10^{-4}	3×10^{-5}	8.0×10^{-5}	2×10^{-5}
	L_2	1.1×10^{-7}	2×10^{-8}	-7.0×10^{-8}	2×10^{-8}
Tb	L_0	1.3059×10^1	3×10^{-3}	9.565×10^0	2×10^{-3}
	L_1	1.9×10^{-4}	1×10^{-5}	6.4×10^{-5}	9×10^{-6}
	L_2	9.0×10^{-8}	9×10^{-9}	-6.7×10^{-8}	7×10^{-9}

Note: Note that the ATEC can be expressed by $\alpha = 1/L_0 \, dL/dT = 1/L_0 (L_1 + L_2T)$.

^aThe 2nd order coefficients, L_2 , for the a -axis of Tm and Yb are meaningless. As shown in Figure 5, they show an almost linear line.

dL/dT_T) of the a - and c -axis were calculated using the coefficients of L_0 , L_1 and L_3 .

Results

Sample and thermal analysis

The prepared sample powders were generally white in color except for the samples with $R = \text{Er}$, which was pink, $R = \text{Tb}$, which was brownish, and $R = \text{Ho}$, which was orange. No significant signals that indicate weight increase or decrease were observed in the TG analysis for all the samples, and the endothermic/exothermic peaks of melting, solidification, or phase transition were observed in the DTA signals.

The obtained melting temperatures for $\text{Ba}_3\text{RB}_3\text{O}_9$ compounds ($R = \text{Sm} - \text{Yb}$, and Y) were summarized in Figure 2. They are consistent with the reported values of melting temperature for $R = \text{Dy} - \text{Yb}$ and Y by Cox et al. [2], $R = \text{Y}$ by Li et al. [4, 5], and $R = \text{Tm}$ and Yb by Khamaganova et al. [3], but are inconsistent with those reported for $R = \text{Y}$, Ho , and Er by Khamaganova et al. [3]. It may be noted that the melting temperatures observed during the cooling-down period are different from those during the heating-up period, and the difference reached $\sim 100^\circ\text{C}$ for Dy , in particular. The fact suggests the overcooled state during the cooling-down period. Additionally, the phase transition temperatures fluctuated in each measurement, suggesting the association of thermal hysteresis or kinetics.

X-ray diffraction measurements

The XRD profiles at RT revealed that the samples with $R = \text{Sm} - \text{Tb}$ and with $R = \text{Dy} - \text{Yb}$, Y showed the H type structures and the L type structures, respectively. In the HT-XRD, no phase transition was found for the H-type phase ($R\bar{3}$) with $R = \text{Sm} - \text{Tb}$ (Figure 3(a)) and the L-type phase ($P6_3\text{cm}$) with $R = \text{Tm} - \text{Yb}$ (Figure 3(c)). On the other hand, phase transition from the L phase to the H phase was observed for $R = \text{Dy} - \text{Er}$, and Y at around $1,100 - 1,200^\circ\text{C}$ (Figure 3(b)). It may be noted that the HT-XRD measurement with $R = \text{Dy}$ and Ho did not show phase transition from the H phase to the L phase during the cooling-down period, in particular. The phase transitions for $\text{Ba}_3\text{DyB}_3\text{O}_9$ and $\text{Ba}_3\text{HoB}_3\text{O}_9$ are affected largely by thermal hysteresis or kinetics.

Discussions

The unit cell parameters at room temperature

Figure 4 shows the cell parameters at RT as a function of $r_R + r_O$ (the sum of the effective ionic radius of REE, r_R , and that of oxygen, r_O [12]). The c -axis of the L phase increases significantly with increasing $r_R + r_O$, which is associated with the structural features of the L-phase. The L type structure consists of the stacking the RO_6 layers and BaO_9 layers along the c -axis and the RO_6 and BaO_9 coordination polyhedra link together by sharing a

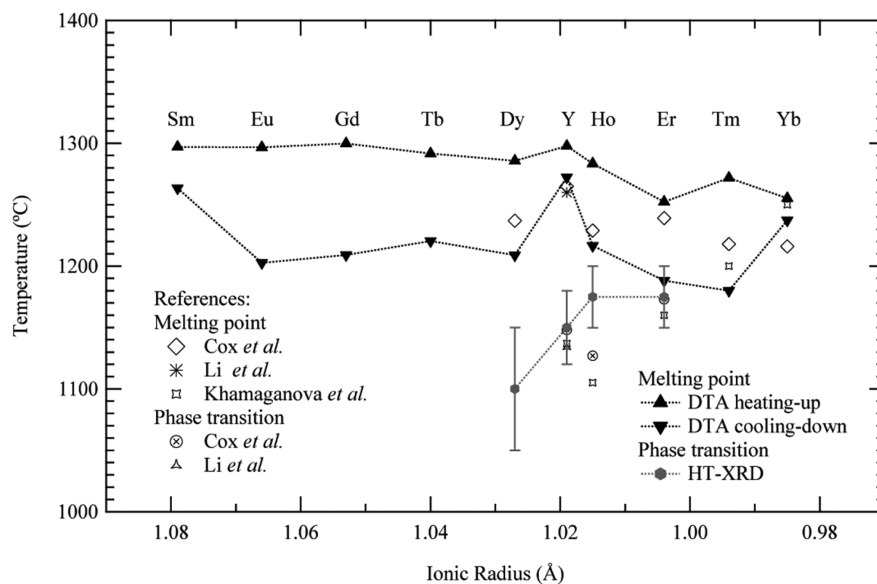


Figure 2: Melting temperatures during heating-up and cooling-down period by DTA and phase transition temperatures during heating-up period by HT-XRD for the $\text{Ba}_3\text{RB}_3\text{O}_9$ system are shown with the published temperatures [2–5]. The horizontal axis is the effective ionic radius of REE [12].

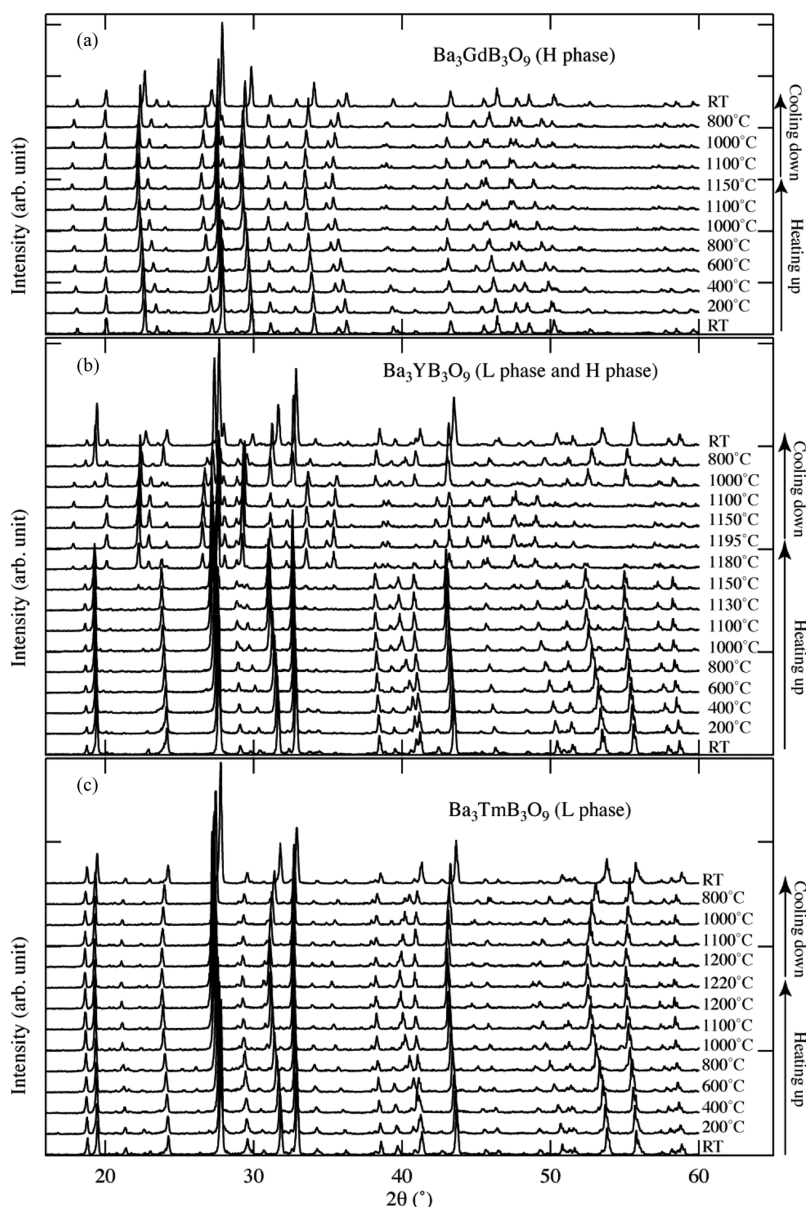


Figure 3: Representative patterns from the three types of typical XRD diffractions for $\text{Ba}_3\text{RB}_3\text{O}_9$; (a) H phase only, $R = \text{Gd}$; (b) H and L phase, $R = \text{Y}$; and (c) L phase only $R = \text{Tm}$. The numbers in the graph show the measurement temperature and RT indicates room temperature.

triangle face. This unique linkage indicates a strong electrostatic repulsion along the c -axis and produces an appreciated effect of the length of the c -axis. In contrast, the no strong anisotropy was detected in the variation of cell parameters for the H phase as shown in Figure 4(a) and (b). These features are associated with the rather homogeneous arrangement of the RO_6 and BaO_9 polyhedra in the H-type structure.

Thermal expansion coefficients

Temperature dependences of unit cell parameters are shown in Figure 5, and the data can be approximated by quadratic curves.

In the case of the H phase, the ATEC of the a -axis increases linearly from $\sim 15 \times 10^{-6} \text{ } ^\circ\text{C}^{-1}$ to $\sim 30 \times 10^{-6} \text{ } ^\circ\text{C}^{-1}$ and that of the c -axis decreases linearly from $\sim 10 \times 10^{-6} \text{ } ^\circ\text{C}^{-1}$ to $\sim -10 \times 10^{-6} \text{ } ^\circ\text{C}^{-1}$ as a function of temperature. This anisotropic thermal expansion for the H phase can be attributed to the distribution of BO_3 triangles and their thermal vibration at the high temperature [13–16]. The normal vectors of BO_3 triangles are almost perpendicular to the c -axis, as shown in the close-up figure of the H phase (Figure 6(a)) and then the expected thermal vibration of BO_3 triangles perpendicular to the plane of the triangle encourages the larger ATEC of the a -axis in the present case.

On the contrary, the ATEC for the a -axis of the L phase decreases linearly from $\sim 10 \times 10^{-6} \text{ } ^\circ\text{C}^{-1}$ to $\sim 5 \times 10^{-6} \text{ } ^\circ\text{C}^{-1}$ with

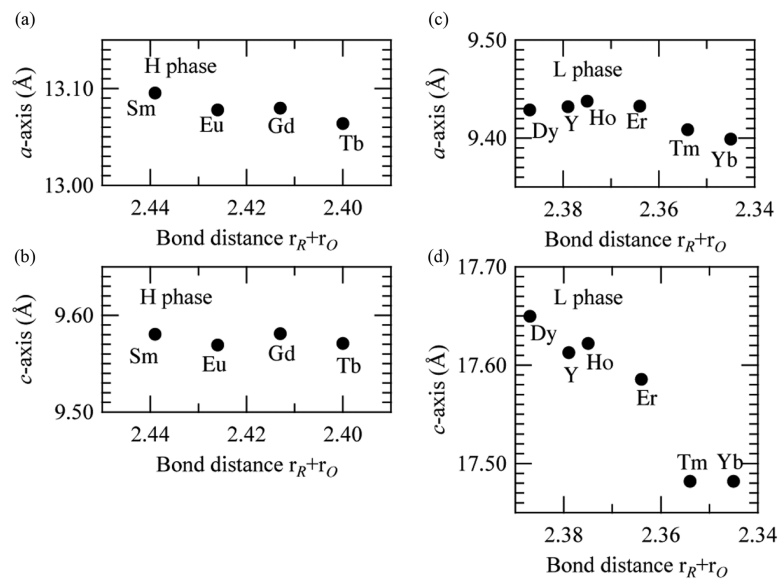


Figure 4: The unit cell parameters versus the sum of the effective ionic radius ratio, $r_R + r_O$, at room temperature; (a) a - and (b) c -axes of the H phase, and (c) a - and (d) c -axes of the L phase. Note that horizontal axes are reversed.

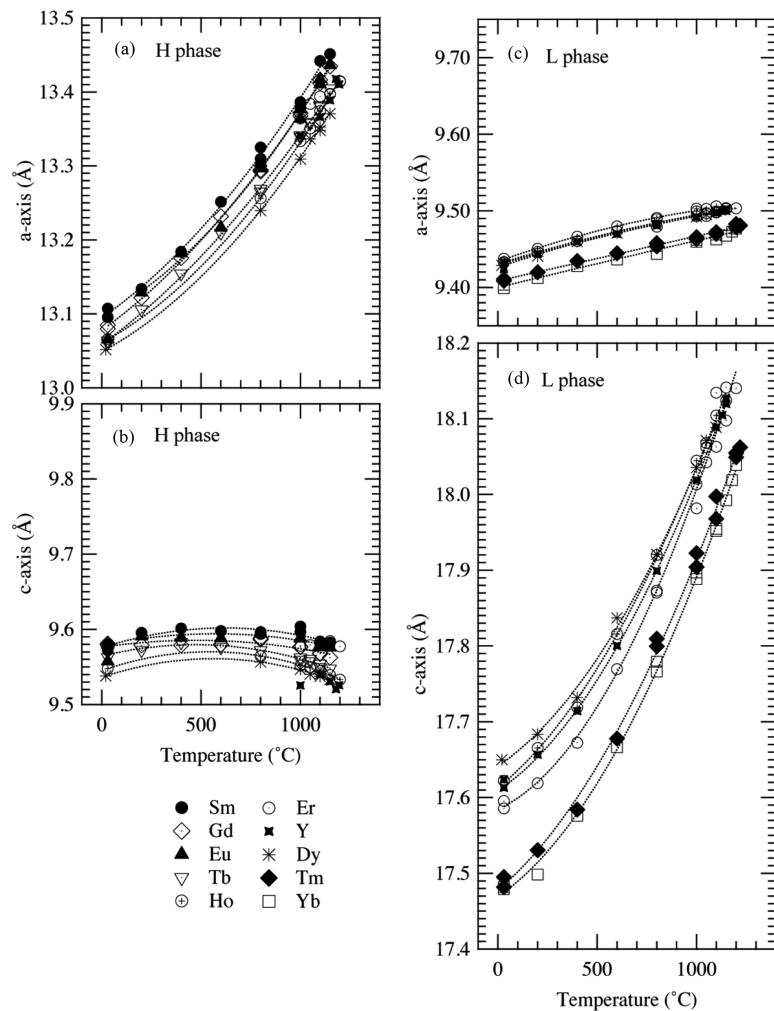


Figure 5: Temperature dependence of the unit cell parameters; (a) a - and (b) c -axes of the H phase, and (c) a - and (d) c -axes of the L phase. Dotted lines are the fitted quadratic curves. Fitted coefficients are shown in Table 1.

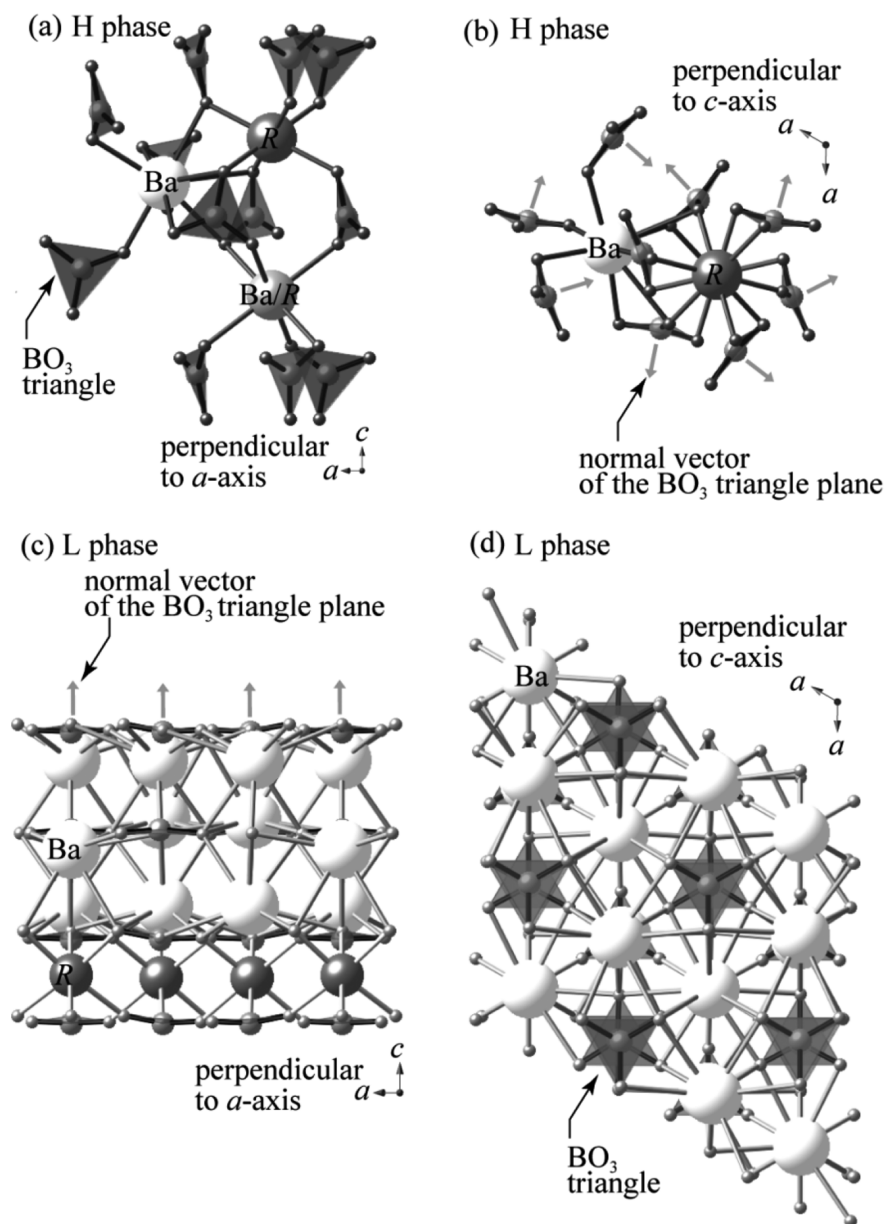


Figure 6: Crystal structure of $\text{Ba}_3\text{RB}_3\text{O}_9$ focused on the direction of the BO_3 triangles illustrated in black triangles. Structures perpendicular to the (a) a - and (b) c -axes of the H phase and those perpendicular to the (c) a - and (d) c -axes of the L phase are shown.

increasing temperature, and increases linearly from $\sim 10 \times 10^{-6} \text{ }^\circ\text{C}^{-1}$ to $\sim 40 \times 10^{-6} \text{ }^\circ\text{C}^{-1}$ for the c -axis. This anisotropy can be discussed by using the structural features found in the alignment of BO_3 triangles, again. As shown in Figure 6, the planes of BO_3 triangles are perpendicular to the c -axis, and the anisotropic thermal vibration of the BO_3 triangle could be associated with the larger ATEC along the c -axis. Similar distribution of BO_3 triangles was also reported in the structure of LuBO_3 (calcite modification), and the larger thermal expansion perpendicular to the BO_3 triangles was demonstrated [13].

Summary

Features of the phase transition in the $\text{Ba}_3\text{RB}_3\text{O}_9$ ($R = \text{Sm}$ – Yb , and Y) systems were examined using TG-DTA and HT-XRD. The $\text{Ba}_3\text{RB}_3\text{O}_9$ ($R = \text{Sm}$ – Tb) system with the lighter REE indicates no solid–solid phase transition and remained as the H phase up to the melting temperature. The system ($R = \text{Tm}$ – Yb) with heavier REE also indicates no solid–solid phase transition, and they remained as the L phase. In contrast, the system ($R = \text{Dy}$ – Er , and Y) shows a solid–solid phase transition from L-type to H-type phases.

Features of the thermal expansion coefficient for the $\text{Ba}_3\text{RB}_3\text{O}_9$ ($R = \text{Sm}$ – Yb , and Y) systems were investigated by the HT-XRD measurements. The ATEC of the a -axis for the H phase was larger than that of the c -axis. On the contrary, the ATEC of the c -axis for the L phase was larger than that of the a -axis. These anisotropic thermal behaviors are associated well with the systematic distribution of the BO_3 triangles in the crystal structures. The larger thermal expansion is realized in the direction perpendicular to the planes of BO_3 triangles and this feature is in accordance with the thermal vibration of BO_3 triangle.

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