Research Article

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Adsorption synergy electrocatalytic degradation of phenol by active oxygen-containing species generated in Co-coal based cathode and graphite anode

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Abstract: The coal base electrodes and efficient coal base loaded cobalt electrodes (Co-CE) were prepared by pyrolysis method of low rank coal united activation method of KOH in order to develop more pores structures. The morphology of electrodes were characterized by Scanning electron microscopy, meanwhile, the type of elements were detected by energy dispersive spectroscopy (EDS). The electrochemical performance of electrodes were tested by cyclic voltammetry and electrochemical impedance spectroscopy. The lamella structures and pores were observed in microtopography of electrodes and the cobalt were successfully loaded in Co-CE from the EDS analysis. The operating conditions of processing time, current density, electrolyte concentration, pH and initial phenol concentration on this electrochemical system in single factor experiment were separately explored, correspondingly, the value was 180 min, 40 mA·cm $^{-2}$, 0.01 mol·L $^{-1}$, 2, 100 mg·L $^{-1}$, and the phenol removal rate (R) were at the range of 47.64-67.84%. In the optimization experiment of JMP design, the removal rate could reach at 83.47%. The response surface methodology was employed for optimizing operation conditions to improve R. And the prediction model obtained for the response can be represented as: $R = 66.5275 + 6.7311X_1 - 5.4197X_4 - 5.2303X_5$ $+4.9555X_1^2 - 12.5219X_2^2 - 6.2912X_4^2 + 16.0937X_5^2 + 2.4109X_2X_4 7.910X_3X_4 - 3.0123X_3X_5 - 2.183X_4X_5$. The optimized conditions were pH 3, 100 mg·L⁻¹ of phenol concentration, 0.1 mol/L of electrolyte concentration, 35 mA/cm² of current density, and 180 min of processing time. Meanwhile, the predicted *R* was 90.86%, the actual *R* of three parallel experiments were 91.2%, 89.3%, 91.05%, which were well consistent with the predicted value. Additionally, the degradation mechanism was proposed as that the adsorption in pore structures synergy electrocatalytic effect of Co-CE. Micro-electric fields formed in pores and the transition metal catalysis accelerated the transformation of cathode hydrogen peroxide to generate hydroxyl radical (·OH). Furthermore, the ·OH were produced both by cathode and anode which promoted the degradation of phenol. This high catalytic activity and low cost Co-CE is a kind of prospective electrode for electrochemical degradation of phenolic wastewater.

Keywords: wastewater, electrode, phenol, response surface methodology, coal based electrode

American government conference of indus-

Abbreviations

ACGIH

	trial hygienists
ANOVA	Analysis of Variance
AOPs	Advanced oxidation processes
AR	Analytical reagent
CCD	Central composite design
CE	Coal based electrode
CEM	Coal based electrode materials
Co-CE	Coal base loaded cobalt electrode
Co-CE-Hy	Co-coal based electrode loaded with Co by
	hydrothermal method
Co-CE2	Co-coal based electrode added with 2% cobalt
	nitrate powder tablet
Co-CE5	Co-coal based electrode added with 5% cobalt
	nitrate powder tablet

Cyclic voltammetry

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CV

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DCLR Direct coal liquefaction residue

 $\begin{array}{ll} D_f & \quad \ \ \, \text{Degrees of freedom} \\ \text{DSA} & \quad \ \ \, \text{Dimension stable anode} \end{array}$

EDS Energy dispersive spectroscopy

EIS Electrochemical impedance spectroscopy

EPA Environmental protection agency

Gr Graphite electrode
OCP Open circuit potential
OEP Oxygen evolution potential

OH Hydroxyl radical R Removal rate

R² Correlation coefficient

RSM Response Surface Methodology R_{ct} charge transfer resistance SCE Saturated calomel electrode SEM Scanning electron microscopy

SJC Sunjiacha coal mine

1 Introduction

As the simplest phenolic compound, phenol was first recovered from coal tar, and most of it was prepared by sulfonation, cumene and other synthetic methods [1]. Phenol is not only an important chemical raw material, also has been widely used in industries such as petroleum industries, oil refining, pharmaceutical industry [2]. According to classification of Environmental protection agency, phenolic compounds were classified as the primary pollutants [3]. The American government conference of industrial hygienists set the standard of phenol exposure limit as 100 ppm. Due to its high toxicity, a small amount of phenol does great harm to people and animals, phenol removal is of great significance for environmental protection treatment and wastewater utilization [4]. The widespread demand for phenol in industry and the increasingly stringent national discharge standards for phenol-contain wastewater, determines phenolic wastewater treatment technology is facing great challenges [5].

Electrochemical method has great significance for industrial wastewater treatment and has been successfully applied for many kind of refractory wastewater [6]. Phenolic wastewater was treated using manifold process like adsorption, chemical method, biological degradation, photocatalysis and Advanced oxidation processes (AOPs) [7,8]. The adsorption has been identified as a promising method due to its simplicity and high efficiency, but the adsorbent reuse is relatively difficult to regeneration [9–12]. Although biological treatment is simple in operation and low in energy consumption, it has limited effect on the removal of toxic

refractory substances and cannot completely remove phenolic compounds [13,14]. The chemical oxidation method is easy to operate, but the operation cost is high, and it also easy to cause secondary pollution [15]. The photocatalytic oxidation method has strong oxidation ability and good performance, whereas, the catalyst requirements are high and the recovery is difficult [16,17]. AOPs uses ozone, hydrogen peroxide, UV radiation produce free radical, a strong oxidizer that promote the degradation of refractory organic molecules [18]. Due to the high oxidation potential and non-selective to contaminant, AOPs have high efficiency [19], however, It is also easy to cause energy consumption [20,21], the cost of chemicals and energy is an important issue. Electrochemical oxidation as one of the AOPs, owing the features of low capital cost, simplicity of operation and no secondary pollution, attracted a wide spread attention [7,22]. Electrochemical methods comparative have better environmental compatibility, higher energy efficiency and easier automation [23]. hydroxyl radical (·OH) with strong oxidizing property was produced by electrochemical method. It can efficiently decompose organic pollutants through oxidation reactions, and even completely convert them into harmless inorganic substances [24]. Oxide species play a great role in the oxidative decomposition of pollutants. The formation of OH mainly depends on the electrode materials [22]. Because of its green and efficient characteristics, electrochemical method is considered to be a method with great development potential, and has been deeply explored and studied [25].

The catalytic efficiency of the electrode is improved by doping modification of the electrode [26], Coal based electrode materials (CEM) is a kind of electrode material with great development potential because of its porous, environmental protection and high efficiency. In recent years, although scholars have made great efforts to develop modified electrodes, carbon, metal oxides and other electrocatalysts still limited by the shortcoming of poor stability and high cost [27]. Many scientists are committed to developing cathodes with high catalytic activity and stability for electrochemical advanced oxidation to remove organic pollutants. With the advantages of low cost, rich porosity, high specific surface area and many active sites on the molecular structure of coal, it has been widely used in the fields of catalysis and adsorption [28]. The advantages of corrosion resistance make it stable under acidic conditions through adsorption synergistic electrochemical degradation of benzene.

Transition metals have become a research hotspot in the field of electrochemistry because of their variable valence state and strong redox ability [29]. The coal base electrodes (CE) can refine the particle size of the electrode by doping metal ions, the compactness and stability were improved, and the transition metal Co ions were doped to promote the production of ·OH, thereby improving the catalytic activity [30,31]. Li doped an appropriate amount of polyethylene glycol and bismuth into the active layer of lead dioxide, which significantly improved the catalytic oxidation performance. The degradation rate of phenol by the prepared electrode was 1.57 times than that of the pure lead dioxide electrode [32]. Yu Zhiyong [33] found that the introduction of Co ions into the Li₂MoO₃ lattice can reduce the particle size of the cathode material, so the doping operation of Co improved the structural stability of the material and reduces the impedance, thereby improving the electrochemical stability of the material is very important. Wang Ying [31] also insisted that the doping of Co can reduce the particle size of PbO₂ and increase the lifetime of PbO₂, which is beneficial to improve the electrocatalytic activity. After the addition of cobalt hydroxide to nickel hydroxide, the mechanical properties have been greatly improved. Even after the charge-discharge cycle, the particle size of the active material in the cobalt-containing electrode is still smaller than that in the cobalt-free electrode. Thereby it is necessary to improve the surface utilization of the active material. When the cobalt content in the active material is not less than 5%, the brittleness is small and the sensitivity to the generated stress is low, which can prolong the cycle life of material [34]. Chang [35] found that direct incorporation of cobalt into the prepared electrode will greatly increase the utilization rate of the active material and increase the average discharge voltage of the battery. And the effect increases with the increase of cobalt content. Among them, the 5 wt% cobalt electrode exhibits the highest average discharge voltage, and further increase of cobalt content has limited performance improvement.

Response surface methodology (RSM) is a statistical technique based on polynomial equation to fit experimental data. It is one of the effective methods to design experimental conditions [36]. To design and optimized the experiment, RSM were used to design and optimize appropriate statistics for the study process. When a set of responses of interest is affected by multiple variables, compared with the

traditional single-factor statistical method, the RSM method not only the influence of a single variable can be predicted, but also can optimize and model the linear and complex relationship between variables and system response under limited number of experiments [21]. Dargahi used Central composite design (CCD-RSM) modeling to explore the removal of phenolic compounds by the adsorption process of modified adsorbents [9]. The electrochemical experiments were designed by RSM. The Analysis of Variance (ANOVA) results obtained from RSM showed that the removal of tetracycline by electrochemical process could be predicted logically and accurately [20].

Coking wastewater contains a large number of phenolic pollutants, the electrochemical degradation of simulated phenol wastewater was carried out by using coal base loaded cobalt electrodes (Co-CE) as cathode, meanwhile the removal effect of phenol was evaluated. The objectives of this work are: (i) select the potential effect electrode by compare experiments of CE, graphite and Co-CE electrodes. (ii) investigate the effect of pH, processing time, current density, electrolyte concentration and phenol concentration, and optimize the system process by CCD-RSM. (iii) the possible degradation pathway of phenol was proposed based on the behavior of this electrochemical system.

2 Experiment

2.1 Materials and reagents

The raw materials are low rank coal from Sunjiacha coal mine (SJC) and Direct coal liquefaction residue (DCLR) from a coal chemical plant, which were both originated from Yulin, Shaanxi Province. The industrial analysis and elemental analysis of them were shown in the Table 1.

All the chemical drug were commercially available and directly used without further purification. Phenol (AR Grade) was provided by Tianjin Zhiyuan Chemical Reagent Co., Ltd, China. Nitric acid (HNO₃, 65-68%) was supplied by Chengdu Kelong Chemical Reagent Factory,

Table 1: Industrial analysis and elemental analysis of raw materials

Sample		Industrial analysis (%)				Elemental analysis (%)			
	M _t	A _{ad}	V_{ad}	FC _{ad}	C _{ad}	O _{ad}	H _{ad}	N_{ad}	$\mathbf{S}_{t,ad}$
SJC	2.94	4.21	30.51	56.16	76.40	17.60	4.70	1.00	0.30
DCLR	0.14	17.64	33.75	48.37	75.00	17.33	4.72	0.77	2.13

ad: air dry basis; Mt: total moisture; St,ad: total sulfur.

China. Sodium hydroxide (NaOH, \geq 96%) was provided by Tianjin Hedong Hongyan Reagent Factory, China. Sodium sulfate anhydrous (Na₂SO₄, \geq 99.0%)) was purchased from Tianjin Damao Chemical Reagent Factory. 4-Aminoantipyrine (\geq 98.5%) was provided by Sinopharm Chemical Reagent Co., Ltd, China. Ammonium chloride (NH₄Cl, \geq 99.5%)) was provided by Tianjin Sheng'ao Chemical Reagents Co., Ltd, China. Potassium hexacyanoferrate (K_3 (Fe(CN)₆), \geq 99.5%) was provided by Tianjin Tianli Chemical Reagents Co., Ltd, China. Cobalt(π) nitrate hexahydrate (Co(NO₃)₂·6H₂O, AR Grade) was obtained from Guangdong Guanghua Sci-Tech Co., Ltd, China. Ethanol (C_2 H₃OH, \geq 99.7%) was purchased from Tianjin Fuyu Fine Chemical Co., Ltd, China. Ammonia solution (NH₃, AR Grade), Sulfuric acid (H₂SO₄, 95–98%) was purchased from Tianjin Kermel Chemical Reagent Co., Ltd, China.

for overnight [37]. The CoNO_3 were mixed with fine pretreated coal powers in a wight ratio of 5 wt%, Under a pressure of 5 MPa to form a table (ϕ 30 mm × 2 mm) marked as CEM-I. After dried for 24 h, thermal decomposition for 0.5 h at 800°C under a N_2 atmosphere, CEM-II was gained. Immersed in 40% HNO_3 for 8 h [38], washed with distilled water until the wash water was neutral, and after air drying, CEM-III was formed. Annealing at 300°C for 30 min and after air drying, CEM-IV was obtained. The above is the preparation method of Co-coal based electrode added with 5% cobalt nitrate powder tablet (Co-CE5). For comparison, Co-coal based electrode added with 2% cobalt nitrate powder tablet (Co-CE2) was fabricated under similar condition but with 2 wt% CoNO₃ addition. CE was also obtained without cobalt addition.

as an activator solution and dried under vacuum at 120°C

2.2 Preparation of Co-CE materials

The specific diagram of the Preparation flow of Co-CE is illustrated in Figure 1. For a typical run, the SJC and DCLR first ground separately in a planet-wheel ball mill at a rotation, then was sieved to a powder in a diameter of fewer than 120 μ m and mixed in a weight ratio of 4:1. Thereafter, the 10% KOH were added into coal dry material

2.3 Characterizations of electrodes

2.3.1 Structural characterizations

The Co-CE was characterized by Scanning electron microscopy (SEM) and energy dispersive spectroscopy (EDS), in which the surface morphology was observed by SEM

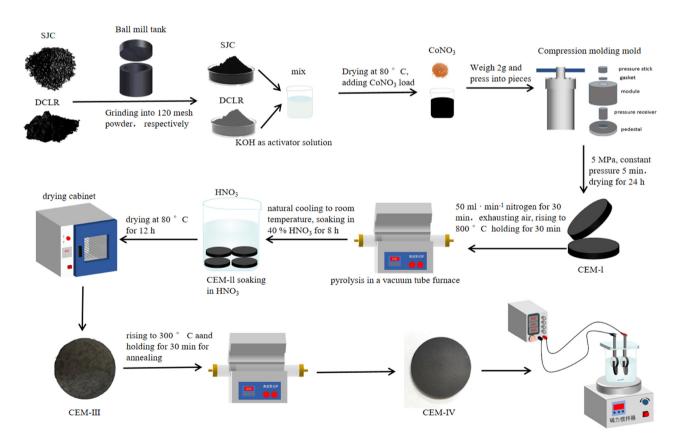


Figure 1: Schematic diagram of preparation of Co-CE.

(Gemini Sigma 300 VP SEM, Zeiss) and the elements on the surface of the doped electrode were analyzed by EDS. Cyclic voltammetry (CV) and electrochemical impedance spectroscopy (EIS) were conducted using an electrochemical workstation (CH1660D, Shanghai). The CV tests were carried out at a scan rate of 20, 50, 100 mV·s⁻¹ in the range of -1.2 to 0 V, and a scan cycle of 50 cycles. The EIS measurement was carried out in a frequency range from 100 kHz to 0.01 Hz with an applied sine wave of 10 mV amplitude at Open circuit potential. All the electrochemical tests were performed in 10 mg·L⁻¹ nitrate aqueous solution and 0.05 mol/L Na₂SO₄ (the Saturated calomel electrode as the reference electrode. the Dimension stable anode electrode as the counter electrode and the prepared electrodes as the working electrode). The absorbance of phenol at a specific wavelength of 510 nm was determined by the 4-aminoantipyrine spectrophotometric method (HJ 503-2009) using a VIS spectrophotometer (722 N, Shanghai Jinghua Technology Instrument Co., Ltd, China) and substituted into the standard curve equation to calculate the concentration of phenol.

2.3.2 Electrochemical experiments

Electrocatalytic degradation of phenol was carried out in a beaker with the working volume of 250 mL, equipped with a magnetic stirrer. The effective dimensions of the Co-CE in solution was 30 mm × 30 mm × 2 mm, and a graphite electrode (Gr) of the same effective area were used as the anode. The catalytic performance of the electrodes was performed in a simulated wastewater solution consisting of 200 mL, 0.05 mol/L Na₂SO₄ and 100 mg·L⁻¹ phenol. At the beginning of treatment, the electrode was immersed in the electrolyte for 30 min to make it fully contact with the simulated solution to reach a stable state. The optimal electrode spacing between the working electrode were analysied in our previous work [39], before the systematic research of the electrode spacing between the electrodes, it was set as 20 mm in this experiment. Otherwise, the phenol wastewater was degraded by a constant current at a current density of 20 mA/cm² for 180 min.

The electrochemical performance of Co-CE was evaluated by phenol degradation rate. The R is calculated by Eq. 1.

$$R = \frac{(C_0 - C_t)}{C_0} \times 100\% \tag{1}$$

where C_0 is the initial phenol concentration and C_t is the phenol concentration at specified time t.

The yield = the (actual) yield of the target product/the theoretical yield of the target product \times 100%. Yield calculation of Co-CE in Eq. 2.

Yield =
$$\frac{m_2}{m_1} \times 100\%$$
 (2)

where m_1 is the mass of electrode plate before the reaction and m_2 is the mass of electrode plate after the reaction.

3 Results and discussion

3.1 Electrode

3.1.1 Electrode treatment process

The efficiencies of the prepared Co-CE were assessed from the weight transformation. As can be observed in Figure 2, gravimetric analysis indicate that the thermal decomposition weightlessness rate is quite high, which is because the presence of oxygenated species in SIC and DCLR, and produced CO₂, H₂O, tars and other volatiles when subjected to high thermal decomposition temperature. With the continuous oxidation of electrode materials by HNO3, new micropores were etched on the electrode. In addition, previous infrared analysis results show that HNO3 treatment can improve the distribution of functional groups on the surface of coal-based electrode. With the extension of activation time, the content of oxygen-containing functional groups such as carboxyl, lactone and phenolic hydroxyl groups on the electrode surface gradually increases, which is also the source of activity in electrochemical reactions [38]. Moreover, the high concentration of HNO₃ will etch the carbon skeleton, resulting in the collapse of the carbon structure surface and the yield will inevitably decrease. This is consistent with the results of SEM analysis, the lamella

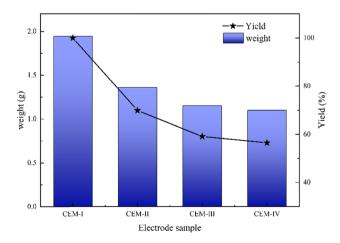


Figure 2: The yield change of electrode preparation process.

structures and pores were observed in microtopography of electrodes and the cobalt were successfully loaded in Co-CE.

3.1.2 Analysis of SEM-EDS

The SEM images of prepared two electrodes are shown in Figure 3. It can be seen from Figure 3(a) and (b) that the surface of the unsupported metal CE is observed to have less void structure and the surface is relatively flat. As showed in Figure 3(c) and (d), the Co element is uniformly distributed on the electrode. when treated by ball milling and carbonization process, the coal-based material particles are accumulated with carbon blocks in the sub-micron order, and microporous structures are observed owing to produced CO2, H2O, tars and other volatiles when pyrolyzing the electrode precursor, which would act as the pore-forming agents, thus leading to porous structures. Noted that some generated hole defects generated during the thermal decomposition can anchor active sites. Such microporous structures could cat as ion-buffering reservoirs, by increasing the ion transport channel to accelerate the penetration of electrolyte, and contribute to improved

electrochemical performance. In addition, the elemental compositions of CE and Co-CE were revealed by element analysis, the detailed contents of which are showed in Figure 3(b) and (c), the result confirmed the existence of the metallic Co array on the coal-based support. It should be pointed out that concentrated HNO₃ has efficiently washed off the interference metal and impurity.

3.1.3 Analysis of CV and EIS

The effects of the added of Co on the electrochemical properties of the CE are studied. In order to evaluate the charge transfer effect of the electrode, EIS tests were carried out. The original curve and the fitted curve have been shown in all EIS plots. It can be seen that the EIS Nyquist diagram mainly includes the semicircle part of the high frequency region and the straight line part of the low frequency region. From Figure 4(a) and (b) it can seen that the Co enhanced the interaction of investigated compounds and the CE, indicating the Co would reinforce positive effect of increasing and activating active sites. The results of the increase in electrocatalytic activity were attributed to the

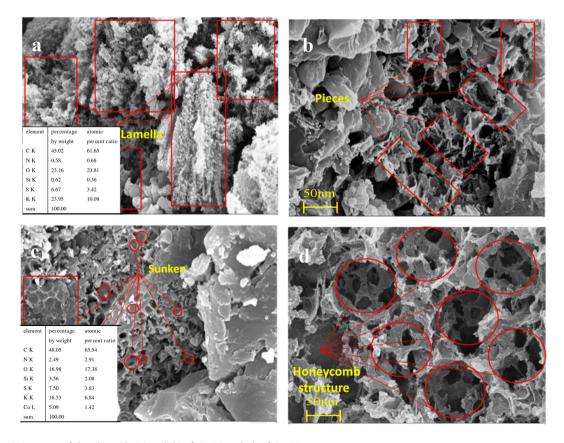


Figure 3: SEM images of the electrode (a) and (b) of CE, (c) and (d) of Co-CE.

changes in the structure and morphology of the Co-CE surface by chemical bonding of Co, which can affect the growth of grain. Cobalt doping increases the pore structure of the electrode material, which is beneficial to the electron transport inside the electrode, reduces ${\rm Co^{3^+}}$ to ${\rm Co^{2^+}}$, promotes the oxidation and reduction of cobalt, releases ·OH, and forms a stable cycle. Appropriate Co doped would also decrease the electrode's electrochemical impedance and the diffusion impedance. The degrees of freedom ($R_{\rm ct}$) is related to the semicircle diameter of the EIS curve. With the decrease of the semicircle diameter of EIS curve, the charge transfer efficiency of the electrode is higher [40]. Clearly, the semicircle diameter of Co-CE on EIS curve was significantly smaller than that of CE. It demonstrated that Co-CE exhibited higher electron transfer ability in

electrochemical oxidation, which was quite consistent with the results of CV tests.

CV curves at different scan rates are tested to further explore their kinetic behaviors. Figure 4(c) and (d) shows the same pattern of CV corresponding to phenol on the electrode materials (CE, Co-CE), no obvious peak could be seen from the CV curves because of the characteristics of coal-based materials themselves. The CV curves of CE and Co-CE are fully preserved and show similar potential when the scan rate increases from 20 to 100 mV·s⁻¹, implying good reversible property of the electrode. The Co-CE had an oxygen evolution potential (OEP) higher than CE, which suggested that the electrochemical catalytic performance of Co-CE was sightly higher than CE, The higher OEP is desirable because it reduces the occurrence of oxygen

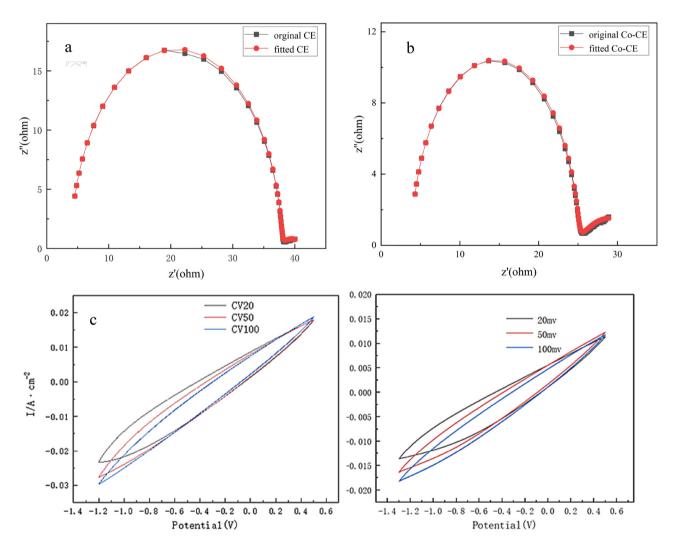


Figure 4: Electrochemical testing of electrodes: (a) EIS Nyquist curves of CE (In 0.05 M Na_2SO_4), (b) EIS Nyquist curves of Co-CE (In 0.05 M Na_2SO_4), (c) CV curves of CE (In 0.05 M Na_2SO_4 and 0.1 g·L⁻¹ phenol at a scan rate of 20, 50, 100 mV·s⁻¹), (d) CV curves of Co-CE (In 0.05 M Na_2SO_4 and 0.1 g·L⁻¹ phenol at a scan rate of 20, 50, 100 mV·s⁻¹).

evolution reaction and is beneficial to the oxidation of organic matter by ·OH.

3.2 Selection of electrodes from removal rate of different electrodes

The phenol solution was electrolyzed using different electrodes under the experimental conditions of a current density of 20 mA/cm² and an electrolyte of 0.05 mol/L anhydrous sodium sulfate. The electrodes include Gr, unsupported CE, Co-coal based electrode loaded with Co by hydrothermal method (Co-CE-Hy), Co-CE2, and Co-CE5.

Table 2 shows the R of phenol, respectively, with 180 min for different electrodes, it can be obtained that the anode using Gr is better than the CE. The cathode using the Co-CE5 is better than the Co-CE-Hy. The Co-CE-Hy loaded with the reactor can only be loaded on one side of the electrode and the loaded is easily shedding. The load layer will fall off when it encounters water, and the effect is not as good as the CE with cobalt nitrate powder. When the amount of cobalt nitrate added reaches 5%, the removal rate of volatile phenol in phenol reaches 47.64%. The results of previous studies show that the electrode degradation effect is different with different Co loading methods. When the loading is less than 5%, the electrode performance improved with the increase of Co loading. Therefore, the graphite electrode was used as the anode and the Co-CE5 was used as the cathode to explore the effect of Co-CE on the electrochemical removal of phenol.

The Co-CE5 material has the highest degradation efficiency and the best degradation performance for phenol, which is consistent with the electrochemical test results and the previous characterization results. It shows that the combination of Co and CEM can produce more electrocatalytic active sites, accelerate the reduction process of O₂, promote the conversion of hydrogen peroxide to ·OH, and improve the degradation rate of phenol. There is a certain

Table 2: Effect of different electrodes on electrochemical treatment of phenol

Anode	Cathode	R (%)
CE	CE	21.43
CE	Co-CE-Hy	27.17
Gr	CE	30.61
Gr	Co-CE-Hy	41.24
Gr	Co-CE2	38.75
Gr	Co-CE5	47.64

gap in the degradation effect of composites with different Co contents, indicating that it is very important to select the appropriate composite ratio.

3.3 Effects of parameters on the degradation of phenol

3.3.1 Effect of electrolysis time

Figure 5 show the various variable parameters of the electrocatalytic degradation of 200 mL phenol by the Co-CE. Figure 5(a) shows after decorated with Co, the Co-CE shows a good activity for activation, and \sim 48% phenol could be degraded in 180 min. The *R* increased slowly at 90–120 min, probably because the *R* increased, the electrocatalytic reaction generated more intermediate products, and the intermediate products could compete with phenol. The effect slows down the growth of phenol degradation rate. The *R* increased slowly at 150–180 min, because with the removal of phenol, the concentration of phenol in the solution decreased, the contact with \cdot 0H was reduced, and the increase of *R* was reduced.

3.3.2 Effect of current density

Current density is an important factor affecting phenol degradation. As shown in Figure 5(b), when no electric voltage is adopted, low R (15.73%) for 100 mg·L⁻¹ phenol solution are observed after 180 min treatment. When improving current density, the R gain obvious improvement owing to the cooperative oxidization processes of the reactive free radicals and adsorption. When the current density was 5, 10, 20, 30 and 40 mA/cm², the R of phenol were 40.64%, 41.04%, 44.21%, 44.63%, 47.64%. Appropriately increasing the current density can not only enhance the adsorption electrosorption capacity, but also accelerate the electron transport, rapidly reduce O2 to produce more H2O2 and ·OH, thereby improving the efficiency of pollutant removal [25]. Further improving the current density to 50 mA/cm², the R at 180 min instead decreases (42.47%), Excessive current density will cause side reactions such as electron reaction (Eq. 3), hydrogen evolution reaction (Eq. 4) and decomposition reaction (Eq. 5) in the electrocatalytic system, resulting in more intermediate products. The gas generated by the side reaction brings stirring to the solution, resulting in a decrease in the thickness of the diffusion layer, thereby reducing the mass transfer coefficient, thus hindering the conversion of H_2O_2 to $\cdot OH$

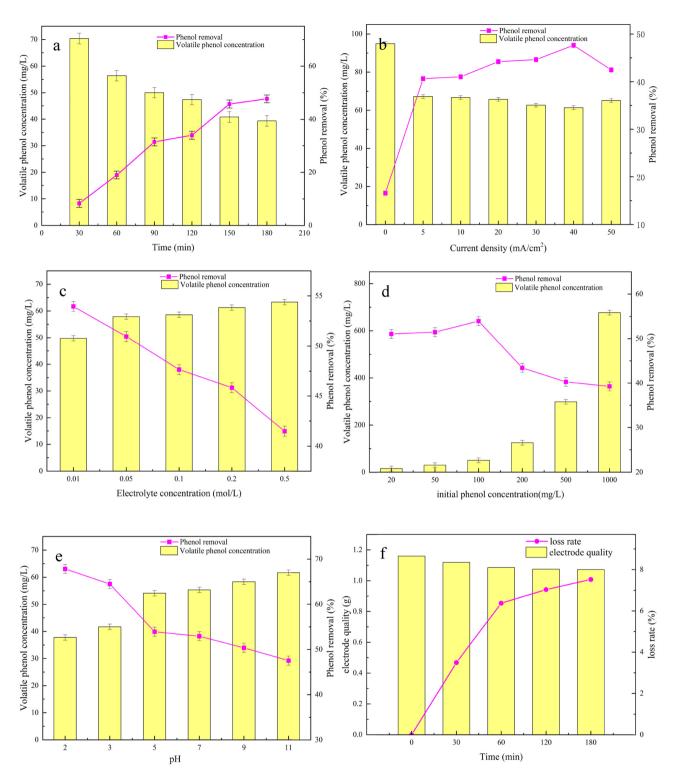


Figure 5: (a) Effect of electrolysis time (20 mA·cm⁻² in 100 mg·L⁻¹ phenol with 0.05 mol·L⁻¹ Na₂SO₄); (b) effect of current density (100 mg·L⁻¹ phenol with 0.05 mol·L⁻¹ Na₂SO₄); (c) effect of Na₂SO₄ concentration (40 mA·cm² in 100 mg·L⁻¹ phenol); (d) effect of initial concentration (40 mA·cm⁻² in 0.01 mol·L⁻¹ Na₂SO₄); (e) effect of pH (40 mA·cm⁻² in 100 mg·L⁻¹ phenol with 0.01 mol·L⁻¹ Na₂SO₄); (f) mechanical stability test.

during the degradation process. At the same time, excessive current will also cause the increase of resistance value in the system, thus affecting the degradation effect of phenol. In this experiment, the optimal current density for phenol degradation was 40 mA/cm².

$$O_2 + 4H^+ + 4e \rightarrow 2H_2O$$
 (3)

$$2H^+ + 2e \rightarrow H_2$$
 (4)

$$2H_2O + 4e \rightarrow O_2 + 4H^+$$
 (5)

3.3.3 Effect of electrolyte concentration

The relationship between electrolyte and conductivity is very close, which has an important influence on the degradation of pollution. Studies have shown that the electrolyte concentration will significantly affect the performance of electrochemical treatment of organic wastewater. As shown in Figure 5(c), with the increase of electrolyte concentration from 0.01 to 0.5 mol/L, the R of phenol decreased from 53.95% to 41.47%. The phenomenon can be explained by that the excess Na₂SO₄ will cover the surface of the electrode, and block the pores, resulting in the decline of R. Although the high concentration of Na₂SO₄ can improve the conductivity of the solution, excessive Na₂SO₄ will lead to the adsorption of SO_4^{2-} anions on the electrode surface, covering some active sites on the electrode surface and resulting in less ·OH formation. In addition, the activity of ·OH is high but the life is very short. The reduction of active sites will hinder the reaction of OH with phenol adsorbed on the electrode surface and reducing the degradation efficiency of phenol [7].

3.3.4 Effect of initial phenol concentration

The *R* of adsorption coupled with the electrochemical reduction process at different phenol concentrations are provided in Figure 5(d). It can be found that with the increase of the phenol concentration from 20 to 100 mg·L⁻¹, the *R* increased from 51.06% to 53.95% at 180 min. This is because when the initial concentration of phenol is low, a sufficient amount of ·OH can oxidize phenol. The increase of concentration helps the diffusion of phenol, and the free radicals fully contact with the pollutants, thereby accelerating the degradation rate of phenol [7]. Above 100 mg·L⁻¹, removal after 180 min treatment show a decline trend. This is because the electrochemical degradation ability of the electrode is limited when facing an aqueous solution with a high concentration of phenol. At the same current density, the number of

strong oxidizing groups generated during the electrolysis process remains unchanged. For the same number of active species, the change of degradation rate increases with the increase of the number of organic molecules. With the degradation of some phenol, a large number of intermediate products will be produced. Due to the non-selective oxidation of ·OH, the competition between phenol and other intermediate products is fierce, and the oxidation reaction of active particles becomes more complicated, which reduces the degradation rate [41].

3.3.5 Effect of pH

The influence of the pH on the degradation efficiency depends on several factors, such as the type of oxidizing species and its oxidizing ability. In order to avoid the contamination of foreign anions, dilute H₂SO₄ and NaOH solutions were used for pH adjustment. Figure 5(e) shows the effect of initial pH on the degradation of phenol in the range of 2-11. A change in the pH from acidic to alkaline pH reduced the R of phenol from 67.84% to 47.54% for 180 min. The maximum R was obtained at pH 2. A decreasing trend of the R was observed above pH 2. According to the previous literature reference [42,43], this phenomenon may be due to the decrease of OEP with the increase of pH. The higher OEP value under acidic conditions weakens the side reaction of oxygen evolution and promotes the indirect catalytic degradation of phenol by ·OH. Under alkaline conditions, ·OH shows weaker reactivity, and has stronger oxidation ability under acidic conditions than under alkaline conditions.

3.3.6 Stability test of Co-CE

Stability is the key factor to determine the application of Co-CE. Stability of the Co-CE for phenol removal was analyzed through the repetitive experiments for phenol removal and was show in Figure 5(f), which was tested by ultrasonic oscillation. Weight loss rate of phenol in every 30 min were 3.49%, 6.37%, 7.30%, 7.52%, respectively. Besides, the Co-CE maintained the same structure after 180 min reaction. The total loss rate in each cycle were lower than 10%, indicating that the structure of Co-CE is relatively stable, and there is a certain weight loss, which can be controlled within 10%. Because the electrode is prepared by pressing the pulverized coal, there is a phenomenon of particle shedding during the electrolysis process. Through multiple sets of experimental verification, as shown in Table 2, when the electrode stability is 15%, the

Table 3: Effect of loss rate on phenol removal process

Loss rate (%)	R (%)
15.00	88.30
13.20	88.65
10.74	89.02
8.35	89.73

removal effect can reach 88.3%. The loss rate is determined to be less than 10%, thus, there will be a higher *R*. The above results suggested that Co-CE maintained a satisfying stability (Table 3).

3.4 Process optimization by RSM

3.4.1 Statistical analysis

The RSM was used to design the required experiments to determine the optimal conditions and the effects of independent variables on the response performance of the electrochemical process (phenol removal). According to the results of single factor experiment, the experimental area was determined roughly, the further optimal experiment were conducted as Table 4. Factors of A (processing time), B (current density), C (electrolyte concentration), D (pH) and E (initial phenol concentration) were list, as well as the value interval. The results of 21 runs of the experiment were obtained from RSM. It was shown in Table 5 taking R as the response value.

3.4.2 ANOVA and effect test of regression model

The ANOVA results revealed an excellent agreement between the experimental results and predicted values of phenol degradation efficiency. The regression surface model was used to explore and predict the interaction of various process variables on the removal efficiency [44]. The degree of

Table 4: Range of variables

Factors		Level	
	-1	0	1
A (min)	150	180	210
$B \text{ (mA/cm}^2)$	20	35	50
C (mol/L)	0.01	0.05	0.10
D	2	3	5
$E \text{ (mg} \cdot L^{-1}\text{)}$	50.0	100.0	150.0

importance and efficiency of the suggested response model were determined by P-value, Correlation coefficient (R^2), F-value and adjusted R^2 , as described in Table 6.

With the help of the phenol grading removal model proposed by RSM, the phenol removal amount of any combination of five parameters can be predicted within the experimental influence range. The significance and sufficiency of phenol removal factors and their interactions were analyzed by p-test [45]. In this study, all the independent variables such as A, D, E, A^2 , B^2 , D^2 , E^2 , B*D, C*D, C*Eand D^*E have P-values lower than 0.05 are obtained as significant model terms for phenol degradation and obtain a model. The order of these key factors is $C^*D > E^2 > D > A =$ $E > B^2 > D^2 > A^2 > C^*E > B^*D > D^*E$. The factors in the front of the order will have a significant impact on the wastewater treatment experiment. The interaction between the two factors in the two-factor influence factor is obviously not a simple linear relationship. We will analyze it through the quadratic regression surface.

3.4.3 RSM optimization and verification

The response of *R* was determined to study the influence of process operation variables over the response. The RSM was used to analyze the experimental data in Table 4. After

Table 5: Design of experiment and experimental response for electrochemical reduction runs

Α	В	С	D	E	R (%)
0	0	-1	-1	0	59.11
1	1	1	1	1	54.94
-1	1	0	-1	1	61.69
0	1	0	1	-1	67.6
0	-1	0	0	0	53.52
0	0	1	0	0	63.22
1	-1	-1	-1	1	76.15
1	0	0	-1	0	76.87
-1	-1	0	-1	-1	76.40
1	0	-1	1	0	77.74
1	-1	1	1	-1	68.4
0	0	0	0	1	77.27
-1	-1	0	1	1	43.25
-1	1	-1	0	-1	74.29
-1	1	-1	1	1	64.96
1	1	-1	-1	1	77.97
0	-1	1	-1	1	70.06
1	-1	-1	-1	-1	77.61
0	1	1	-1	-1	77.19
1	1	1	0	-1	83.47
-1	-1	-1	1	-1	70.05
	0 1 -1 0 0 0 1 1 1 -1 1 0 -1 -1 1 0 1	0 0 1 1 1 -1 1 0 0 -1 -1 1 1 0 -1 1 1 0 1 1 1 0 1 1 1 1	0 0 -1 1 1 1 0 0 1 0 0 1 0 0 -1 0 0 0 1 1 -1 0 0 0 1 1 -1 -1 1 0 0 0 -1 -1 1 0 0 0 -1 -1 1 1 -1 1 0 0 0 -1 -1 1 1 -1 1 1 1 -1 1 1 1 -1 0 -1 1 1 1 1 1 1 1 1 1 1 1	0 0 -1 -1 1 1 1 1 -1 1 0 -1 0 1 0 1 0 0 1 0 0 0 1 0 1 -1 -1 -1 1 0 0 -1 1 0 -1 1 1 0 0 0 -1 -1 1 1 0 0 0 0 -1 -1 0 1 -1 1 -1 0 -1 1 -1 1 1 1 -1 -1 1 1 -1 -1 1 -1 -1 -1 1 -1 -1 -1 1 -1 -1 -1 1 -1 -1 -1 1 -1 -1 -1 1 -1 -1 -1	0 0 -1 -1 0 1 1 1 1 1 -1 1 0 -1 1 0 1 0 0 0 0 0 1 0 0 0 0 1 0 0 0 0 1 0 0 1 -1 -1 1 1 1 0 -1 -1 1 1 1 0 0 0 1 -1 -1 1 0 0 0 0 1 -1 -1 -1 1 -1<

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Table 6: ANOVA results for coefficient of quadratic model for phenol removal

Source	DF	Sum of	Mean	<i>F</i> -value	<i>P</i> -value
		squares	square		
Model	17	2062.8486	121.344	25.4151	0.0108*
Α	1	370.71903		77.6460	0.0031*
В	1	1.70661		0.3574	0.5921
С	1	44.72570		9.3677	0.0550
D	1	390.64124		81.8187	0.0029*
Ε	1	369.78176		77.4497	0.0031*
A^2	1	73.32053		15.3568	0.0295*
B^2	1	247.75007		51.8905	0.0055*
C^2	1	0.01542		0.0031	0.9583
D^2	1	107.93647		22.6070	0.0177*
E^2	1	411.13534		86.1111	0.0026*
A*D	1	0.69084		0.1447	0.7290
B*D	1	56.33118		11.7984	0.0414*
C*D	1	423.27825		88.6544	0.0025*
A*E	1	26.66704		5.5853	0.0991
B*E	1	23.19302		4.8577	0.1147
C*E	1	72.74173		15.2355	0.0299*
D*E	1	49.14879		10.2941	0.0490
Pure error	3	14.3234	4.774		
Cor total	20	2077.1721			
$R^2 = 0.993104$	4				
Adjusted $R^2 = 0.954029$					

^{*}Significant influencing factors.

eliminating the insignificant items, a quadratic regression surface model was established to fit the experimental results, which correlates all process parameters [16]. The model equation was obtained for the response can be represented in terms of coded factors as follows:

$$R = 66.5275 + 6.7311X_1 - 5.4197X_4 - 5.2303X_5 + 4.9555X_1^2$$
$$- 12.5219X_2^2 - 6.2912X_4^2 + 16.0937X_5^2 + 2.4109X_2X_4$$
$$- 7.9105X_3X_4 - 3.0123X_2X_5 - 2.183X_4X_5$$

Where $X_1 = (A - 180)/30$, $X_2 = (B - 35)/15$, $X_3 = (C - 0.055)/0.045$, $X_4 = (D - 3.5)/1.5$, $X_5 = (E - 100)/50$. In above equation, as mentioned earlier, R has been employed to show the removal rate (%), and A, B, C, D and E are utilized to symbolize the time, current density, electrolyte concentration, pH and initial phenol concentration, respectively. The codes X_1 , X_2 , X_3 , X_4 , X_5 are used to represent the algebraic expressions of time, current density, electrolyte concentration, initial phenol concentration and pH, so that the variable factor interval is kept within -1 to 1 to express the prediction model.

The three-dimensional response surface diagram can solve the problem of the optimal conditions of the factors, and is mainly used to establish the understanding of the interaction types between variables, which can be used to improve the efficiency of process treatment. Figure 6(a–d)

represents the interaction of two independent parameters in the significant influencing factors. It can be seen from Figure 6(a) that if all other variables are kept unchanged, if pH (2-5) is increased, the degradation rate will increase slightly and then decrease, and the R is the highest when pH is 3. If the concentration of phenol (50–100 mg·L⁻¹) is increased, the degradation rate will decrease first and then increase slightly. It can be seen from Figure 6(c) and (d) that the R is the highest when the concentration of phenol is 50 mg·L⁻¹. Although other conditions remain unchanged, the electrolyte concentration increases (0.01-0.1 mol/L), and the degradation rate decreases slightly. However, compared with Figure 6(c) and (d), it is found that when the two factors interact, the R is the highest when the electrolyte concentration is 0.1 mol/L. In summary, the optimum electrochemical treatment conditions were current density of 35 mA/cm², Na₂SO₄ concentration of 0.1 mol/L, pH = 3, and initial phenol concentration of 50 mg·L⁻¹. The model data showed that the highest R was 90.86% under this condition. Thereafter, there paralleled experiments were performed in the laboratory with the optimal parameters and the R was 91.2%, 89.3% and 91.05%, it is depicted that the predicted values of RSM is very close of experimental values.

3.5 Adsorption synergy electrocatalytic degradation mechanism

Studies have shown that H_2O_2 and OH play an important role in cathodic electrocatalytic oxidation. The direct conversion from H₂O₂ to ·OH is usually difficult [27]. The simultaneous presence of Co²⁺ and Co³⁺ and the redox reaction promote the production of H₂O₂ and ·OH (as follows Eqs. 6 and 7). Studies have shown that, similar to Fe²⁺, Co²⁺ can also in situ activate H₂O₂ decomposition to produce ·OH, and achieved good treatment effect [46]. The H₂O₂ produced by the cathode reacts rapidly with the transition metal element Co²⁺, which promotes the conversion of H₂O₂ to strong oxidizing substances, making phenol more easily mineralized into CO₂ and water. The introduction of Co species not only acts as a catalyst for the redox process, but more importantly promotes the valence cycle. The production of ·OH is increased by accelerating the redox cycle between Co species, thereby achieving enhanced mineralization of phenol.

$$Co^{2+} + H_2O_2 \rightarrow Co^{3+} + \cdot OH + OH^-$$
 (6)

$$Co^{3+} + e^{-} \rightarrow Co^{2+}$$
 (7)

Based on the above analysis, a reasonable electrocatalytic mechanism for removing phenol was proposed.

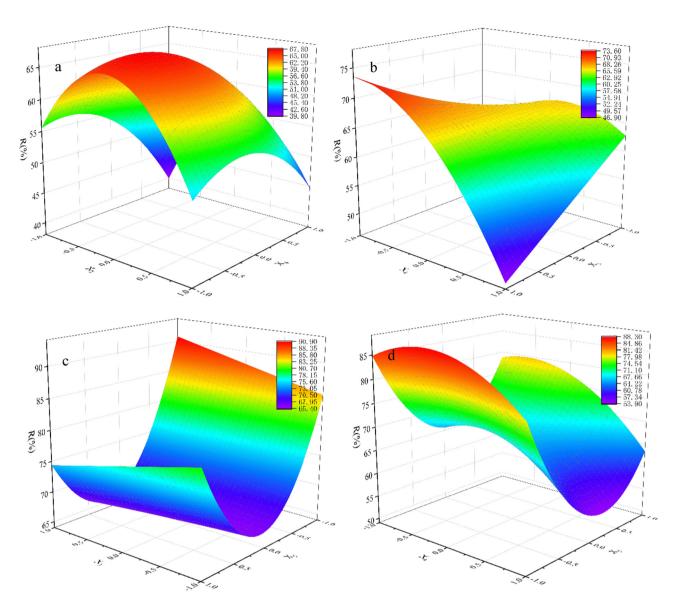


Figure 6: Two-factor response surface diagram: (a) X_2*X_4 , (b) X_3*X_4 , (c) X_3*X_5 , (d) X_4*X_5 .

As a highly effective adsorbent and electrocatalyst, the pores of Co-CE are abundant, forming a micro-electric field in the pores, which promotes the reaction of adsorbed water with oxygen to produce hydrogen peroxide. The porous structure provides more active sites for the reaction and has better degradation effect. The improved electrochemical resulting from Co doping sites and CE hierarchical pores, efficiently facilitate the conversion of H_2O_2 to ·OH. The *in-situ* generated H_2O_2 were catalyzed with Co-CE, and much more ·OH were quickly produced through the active sites of Co(II) on the Co-CE surface. Under the optimal operating conditions, the removal rate obtained by phenol was nearly 91%. Meanwhile, adsorption rate obtained by electrode was 15.73%. There are white adhesions on the cathode

surface, and it is irregularly crystallized, indicating that in addition to adsorption, redox reaction also occurs [47]. Hence, the total phenol removal should be the result of synergistic adsorption and electrocatalytic oxidation.

The mechanism of synergistic adsorption/electrocatalytic oxidation by Co-CE with multi-hole structure was expounded in Figure 7. As above experimental results, For the Co-CE, phenol was first adsorbed on the surface for its multi-hole structure, At the same time, O_2 adsorbed on Co-CE surface is reduced to H_2O_2 by electrons (as follows Eq. 8) and the redox reaction between Co^{2+} and Co^{3+} promotes the conversion of H_2O_2 to ·OH potent oxidizing substances, then, a part of phenol was adsorbed inside the electrode and a part of phenol was effectively oxidized to

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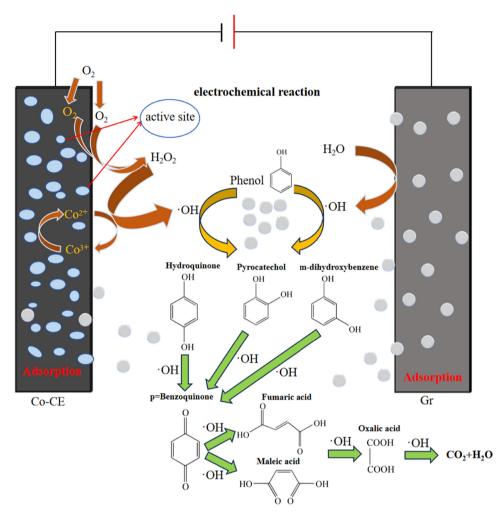


Figure 7: Schematic diagram of phenol degradation mechanism in electrochemical system.

intermediate product, finally was degradation into CO_2 and H_2O . In the electrolytic solution, $\cdot OH$ was produced at both cathode and anode, this makes it easier to mineralize the organic pollutant phenol into carbon dioxide and water. Wang studied the mechanism of electro-oxidation of phenol in aqueous phase based on *in-situ* infrared spectroscopy. It was found that different potentials affected the oxidation products of phenol [48]. Some researchers [7,44,48] believed that phenol was first oxidized to pyrogallol and further changed to quinone, and then oxidized to small molecule acid, which was decomposed into CO_2 and H_2O (as follows Eq. 9). Due to the large potential range of the experiment, it is speculated that both of them exist in the process of electro-oxidation decomposition, and the possible oxidation pathway is shown in Figure 7.

$$O_2 + 2H^+ + 2e^- \rightarrow 2H_2O_2$$
 (8)

$$\cdot$$
OH + Phenol \rightarrow CO₂ + H₂O (9)

4 Conclusion

Co-CE was successfully prepared to study the efficiency of electrocatalytic degradation of phenol. Comparing different electrodes, it was found that graphite as anode, Co-CE5 as cathode had the best phenol degradation effect, and R was 47.64%. The single factor degradation experiments of phenol in simulated wastewater was carried out to determine the following optimal reaction conditions: the time was 180 min, the applied current density was 40 mA/cm², the electrode concentration was 0.01 mol/L, the initial pH was 2, the initial phenol concentration was 100 mg·L⁻¹ and the R were at the range of 47.64-67.84%. The results of ANOVA obtained from RSM showed that the quadratic polynomial model with $R^2 = 0.993$ was suitable and logical for accurate prediction of phenol removal by electrochemical process. The independent variables include A, D, E, Under optimal conditions for time, current density, pH,

electrolyte concentration, initial phenol concentration were 180 min, 35 mA/cm², 3, 0.1 mol/L, 100 mg·L $^{-1}$, the $\it R$ of three parallel experiments were nearly predicting value (91.2%, 89.3%, 91.05%). The redox reaction between $\it Co^{2+}$ and $\it Co^{3+}$ promotes the conversion of $\it H_2O_2$ to ·OH potent oxidizing substances, both anode and cathode produce ·OH, ·OH attacks the benzene ring to degrade phenol, and adsorption synergistic electrocatalysis accelerates the mineralization of pollutants. This high catalytic activity and low cost Co-CE is a kind of prospective electrode for electrochemical degradation of phenolic wastewater. It is also of great significance for industrial application and provides a feasibility for coal chemical wastewater treatment. However, it is in a bottleneck period in achieving large-scale industrial applications.

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