

## Research Article

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# Neural network quaternion-based controller for port-Hamiltonian system

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**Abstract:** In this research article, a control approach for port-Hamiltonian PH systems based in a neural network (NN) quaternion-based control strategy is presented. First, the dynamics is converted by the implementation of a Poisson bracket in order to facilitate the mathematical model in order to obtain a feasible formulation for the controller design based on quaternion NNs. In this study, two controllers for this kind of system are presented: the first one consists in the controller design for a PH system about its equilibrium points taking into consideration the position and momentum. This mean is achieved by dividing the quaternion neural controller into scalar and vectorial parts to facilitate the controller derivation by selecting a Lyapunov functional. The second control strategy consists in designing the trajectory tracking controller, in which a reference moment is considered in order to drive this variable to the final desired position according to a reference variable; again, a Lyapunov functional is implemented to obtain the desired control law. It is important to mention that both controllers take into advantage that the energy consideration and that the representation of many physical systems could be implemented in quaternions. Besides the angular velocity, trajectory tracking of a three-phase induction motor is presented as a third numerical experiment. Two numerical experiments are presented to validate the theoretical results evinced in this study. Finally, a discussion and conclusion section is provided.

**Keywords:** neural networks, quaternions, port-Hamiltonian systems, neural control

**MSC 2020:** 93D15, 93D20, 93D30, 93D05

## 1 Introduction

Due to its energy consideration, port-Hamiltonian systems has become an important mathematical representation for many types of physical systems such as fluid and particle dynamic systems, in which the port-Hamiltonian mathematical representation consists of two phase variables related to the position and the momentum of a particle ensemble. It is important to consider that port-Hamiltonian systems for the representation of mechanical systems have been increased nowadays due to the vast amount of novel robotic mechanisms. For this reason, it is important to obtain a feasible mathematical model for controller design purpose [1,2]. Among the kinds of controllers that can be designed for a port-Hamiltonian system are energy-based and passivity-based control.

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Neural network (NN) control has been implemented nowadays considering the flexibility and easiness to tune for the stabilization of many kinds of nonlinear dynamic systems. For these reasons, in this section, an establishment of the theoretical fundamentals for this study is presented.

NNs have become important nowadays for different kinds of applications that are not necessarily related to controller design. Among these applications, optimization, pattern recognition, classification, and prediction are found; so, for example, in articles like [3], the topological properties of NN from the graph-theory view-point are evinced. Then, in [4], a comparative analysis between feedforward neural-networks and radial-basis NN is performed. Meanwhile, in [5], the stability analysis and control synchronization of NNs are presented. In [6], the Riemannian geometry of deep NNs is shown. Then, in [7,8], an image classification application of convolutional NNs and prediction application is presented, respectively.

Quaternion NNs are crucial for this research study taking into consideration that these type of networks are implemented. The quaternion NNs are divided into a scalar quaternion part and a quaternion vector part. There are several research studies in which these quaternion-based NNs are mentioned: so, for example, in [9], quaternion memristive NNs are analyzed by means of the Lagrangian stability considering that this possesses mixed time delays. Then, in [10], the Mittag-Leffler stability analysis is presented. In [11], a quaternion NN with leakage and proportional delays is analyzed. Then, in [12], a novel synchronization strategy of quaternion-based NNs with time delays is presented. Then, in [13,14], an stochastic version of quaternion NN and the stabilization of quaternion delayed NNs are shown.

NNs have been extensively implemented nowadays in the control and stabilization of nonlinear and many kinds of complex dynamical systems. For example, in articles like [15], the neural control of discrete weak formulation is presented. Then, in [16], the neural control of a space vehicle with output constraints is presented. Meanwhile, in [17], a space manipulator is controlled by means of NN control designed by selecting barrier tan-type Lyapunov functions. Then, in [18], a review of different types of neural controllers for nuclear power plants is presented. Then, in [19,20], two interesting applications of NN control for an underwater vehicle and switched nonlinear interconnected systems are shown.

Dynamic control is important taking into consideration that the type of quaternion-based neural controller is dynamic. So the following references are mentioned taking into consideration that this kind of control strategy is worthy to mention. In references like [21], a dynamic controller for aerobic granular sludge reactor is presented. Meanwhile, in [22], the energy decay of the wave equation by a delay in the dynamic control is evinced. Then, in [23], the control of refrigeration cycle with single, dual, and triple effects is presented. Finally, in [24,25], the design of an adaptive backstepping and NN dynamic control with dynamic surface is presented, respectively.

As mentioned earlier, port-Hamiltonian systems are important to be studied and analyzed considering the energy properties of these kinds of systems. It is crucial to take into consideration that novel control strategies as proposed in this article are necessary considering the complexity of this kind of complex dynamic system. In the literature, there are some research studies regarding this topic such as [26], in which the control with output consensus for PH system is presented. Meanwhile, in [27], the discretization of PH systems by the finite elements is shown. Meanwhile, in [28], the exponential decay rate of port-Hamiltonian system is evinced. It is worthy to cite references like [29], and the port-Hamiltonian derivation for chemical processes is shown. Finally, in [30,31], the mixed geometric coupling of PH system is achieved and the model predictive control of PH systems is presented, respectively.

In this study, the design and synthesis of a quaternion-based NN controller for a PH system is evinced. First, in order to improve the tractability of the port-Hamiltonian mathematical formulation, the PH system is represented by means of the Poisson bracket. The use of this operator makes it easy in order to synthesize the controller for this kind of mathematical model. The NN quaternion-based controller is designed by dividing the quaternion NN into the scalar quaternion and the vector quaternion; so by selecting appropriate control law, the implementation of suitable Lyapunov functionals is done in order to obtain a feasible control law. In this study, two kinds of NN quaternion-based controllers are shown, for either stabilization and trajectory tracking purposes, so in this way, the controller is suitable to be implemented, in order to follow the trajectory of a reference variable or simply stabilizes the port-Hamiltonian system in its equilibrium point. This experiment

consists by selecting the movement of a particle in order to stabilize its trajectory. Discussions and conclusions of the theoretical and experimental results are shown, respectively.

The contributions are shown as follows:

- Considering the complex dynamics of port-Hamiltonian systems, NN controllers are suitable to stabilize and for trajectory tracking control.
- Quaternion NNs are suitable considering that the dynamics of robots and unmanned aerial vehicles, for example, are established in quaternions.
- Quaternion NNs provide more degrees of freedom for control purposes in comparison with other types of NNs.
- The NN controller provided in this research study provides a fast and accurate closed-loop system response.
- This NN controller approach provides an easy-to-tune NNs parameters.

## 2 Related work

In this section, the comparison of the quaternion NNs with other type of NNs is presented considering the advantages and disadvantages. Besides, passivity-based and energy-based control for PH systems is presented taking into account that these control strategies are commonly found.

Quaternion NNs are fundamental in this article, so it is important to mention the following studies. For example, in [32], in which the power law synchronization of quaternion-valued NN is shown. Then, in [11], quaternion-based NNs stabilization with time delays is presented. It is important to consider time delays in quaternion NNs because it is a common phenomenon found in many real physical systems that can produce instability or poor closed-loop performance. Meanwhile, in [33], the stochastic synchronization of Markovian jump quaternion NN synchronization is presented. In [34], the dissipative and synchronization of quaternion-based NNs is shown. Then, in [35], the stability analysis and control of Markovian jump quaternion-based NNs is evinced.

Other types of neural controllers that are useful for this research study are in [36], in which the synchronization of fractional order fuzzy NN is achieved by the implementation of a nonlinear feedback control law. Meanwhile, in [37], a direct current motor is controlled by a fuzzy neural PID control, which is presented in this article. In [38], the state estimation and NN control of a Markovian jump system is presented. Then, in [39], a fractional order NN is presented to control a rehabilitation robot. In [40], a sliding mode controller and a recurrent NN based on a robotic operated vehicle are presented. In [41], a neural controller is designed for the stabilization of a water reactor.

Diverse kinds of controllers have been developed during the past decades, considering that plenty of physical systems in which this controller can be implemented has been discovered. For example, in articles like [42], the observer design for a 1-D parameter-distributed port-Hamiltonian system is evinced. Then, in articles like [43], a fully actuated mechanical system in the PH formulation is controlled by virtual contractivity. In [44], an analysis of reduced model boundary control strategies for linear PH systems is presented. Meanwhile, in [45], a boundary-controlled port-Hamiltonian system is presented. Then, in [46,47], the thermodynamic PH system optimal control and the structure-preserving discretization of PH system are shown.

Energy control of PH systems is considered as one of the important control strategies for PH systems taking into consideration the energy properties of port-Hamiltonian systems; among these important papers found in the literature are papers like [48], in which the design of an energy controller and observer for infinite dimensional PH system is presented. Meanwhile, in [49], an energy controller design in domain control of infinite dimensional PH system is evinced. Then, in [50], the controller design of the PH system with minimal energy supply is evinced. In [51], the structural invariance and control of PH systems are presented. Then, in [52,53], the boundary control based in energy shaping of PH systems and energy-based feedback control of port-Hamiltonian systems is presented, respectively.

To finalize this literature review, consider the following references regarding the control of PH systems based on passivity, in which this dissipative-based control strategy is important to this study, taking into consideration that this strategy is widely used [54–59].

In this paragraph are remarked the differences, advantages, and disadvantages of quaternion NNs in comparison with other types of NNs. In this case, is important to mention the comparison of quaternion NNs with complex variable NNs and fuzzy NNs. In references like [60–62], complex-valued NNs are presented. It is proved that quaternion NNs provide more degrees of freedom for control purposes in comparison with complex variable NNs. So for this reason, the measurement of the performances is significantly superior with the quaternion NN in comparison with complex variable NNs. Besides, taking advantage that the kinematics and dynamics of many robotics and unmanned aerial vehicle systems are represented with the quaternion mathematical definition, it is advantageous to implement the quaternion NNs as presented in this research study.

On the other side in articles like [63–65], fuzzy NNs are presented, the advantages that these kinds of NNs possess are that they are useful for dynamic system with uncertainties, something that the quaternion NNs do not possess these characteristics. It must be recalled that the computational effort of quaternion NNs is significantly low in comparison with other NN strategies, something that is an advantage in real-time applications of neural controllers.

### 3 Theoretical background

In this section, basically the fundamentals of the Poisson bracket and the port-Hamiltonian formulation are explained.

#### 3.1 Poisson bracket

The Poisson bracket is given by [66,67]

$$\partial_t z^A = \{z^A, \mathcal{H}\}, \quad (1)$$

where  $z^A = \{q_1, q_2, \dots, q_N, p_1, p_2, \dots, p_N\}$  is the state vector,  $\mathcal{H}$  is the Hamiltonian, and  $\{.,.\}$  denotes the Poisson bracket. Their properties are:

**Property 1.** The Poisson bracket properties, in which it is defined by  $\{.,.\}$ :

- Anti-symmetry  $\{\mathcal{F}, \mathcal{G}\} = -\{\mathcal{G}, \mathcal{F}\}$ .
- Leibniz rule  $\{\mathcal{G}, \mathcal{F}\mathcal{E}\} = \mathcal{G}\{\mathcal{F}, \mathcal{E}\} + \{\mathcal{F}, \mathcal{G}\}\mathcal{E}$ ,

where  $\mathcal{P}$  is an N-dimensional manifold.

The Poisson bracket is obtained by:

$$\{\mathcal{F}, \mathcal{G}\} = \frac{\partial \mathcal{F}^T}{\partial z} \mathbb{J}(z) \frac{\partial \mathcal{G}}{\partial z}, \quad (2)$$

where  $\mathbb{J}(z)$  is the Poisson matrix.

#### 3.2 Port-Hamiltonian dynamic system formulation

So in order to establish the port-Hamiltonian formulation, consider the state vector  $x = [q, p]^T$  with the following partial derivatives:

$$\begin{aligned} \frac{\partial p}{\partial x} &= [0_n, I_n]^T, \\ \frac{\partial q}{\partial x} &= [I_n, 0_n]^T, \\ \frac{\partial H}{\partial x} &= \left[ \frac{\partial H}{\partial q}, \frac{\partial H}{\partial p} \right]^T. \end{aligned} \quad (3)$$

So consider the following Poisson bracket:

$$\mathbb{J}(z) = \begin{bmatrix} 0 & I \\ -I & -D \end{bmatrix}, \quad (4)$$

where  $I$  is the identity matrix and  $D \in \mathbb{R}^{n \times n}$  is an appropriate matrix. So by implementing the following Poisson matrix is obtained:

$$\begin{aligned} \{p, \mathcal{H}\} &= \frac{\partial p^T}{\partial x} \mathbb{J}(x) \frac{\partial \mathcal{H}}{\partial x} = -\frac{\partial \mathcal{H}}{\partial q} - D \frac{\partial \mathcal{H}}{\partial p} \\ \{q, \mathcal{H}\} &= \frac{\partial q^T}{\partial x} \mathbb{J}(x) \frac{\partial \mathcal{H}}{\partial x} = \frac{\partial \mathcal{H}}{\partial p}, \end{aligned} \quad (5)$$

where  $\mathcal{H}$  is the Hamiltonian. So the PH formulation is:

$$\begin{aligned} \dot{q} &= \{q, \mathcal{H}\}, \\ \dot{p} &= \{p, \mathcal{H}\} + u, \end{aligned} \quad (6)$$

where  $u \in \mathbb{R}^n$  is the control input.

## 4 Stabilization and trajectory tracking of port-Hamiltonian dynamic systems by quaternion-based controllers

Consider the following quaternion-based NN controller:

$$\dot{z} = -A_c z^r(t) + \sum_{r=1}^n d_{pr} f_c(z) + I_c, \quad (7)$$

for the quaternion variable  $z = z^r + iz^i + jz^j + kz^k$  and the function  $f_c(z) = f_c^r + if_c^i + jf_c^j + kf_c^k$ ; meanwhile,  $I_c$  is the neural controller input, and  $A_c$  is a positive definite matrix of appropriate dimension. In this section it is important to remark that the NN architecture for the quaternion NN controller is basically feedforward alike. This means that the quaternion NN controllers possess the input neurons and output neurons with their input and bias weights. This quaternion NN controller possess a nonlinear activation function very similar to the standard feedforward NN architecture. The quaternion operation follows the following properties:

$$\begin{aligned} i \cdot i &= 0, & j \cdot j &= 0, \\ i \cdot j &= k, & i \cdot k &= -j, \\ j \cdot k &= i, & k \cdot k &= 0, \end{aligned} \quad (8)$$

so by separating the scalar quaternion part and the vector quaternion part yields

$$\begin{aligned} \dot{z}^r &= -A_c z^r + \sum_{r=1}^n d_{pr} f_c^r(z) + I_c, \\ \dot{z}^i &= \sum_{r=1}^n d_{pr} f_c^i(z), \\ \dot{z}^j &= \sum_{r=1}^n d_{pr} f_c^j(z), \\ \dot{z}^k &= \sum_{r=1}^n d_{pr} f_c^k(z), \end{aligned} \quad (9)$$

in which the NN parameters are given by the positive definite matrix  $A_c$  and the NN weights  $d_{pr}$ ; similar to the NN parameters as evinced in (7). It is important to remark that (7) and (8) are used to obtain (9). The reason to separate the variables of the quaternion NN is to facilitate the design of the quaternion NN controller in

Theorems 1 and 2 so in this way the control synthesis by the Lyapunov theorem is facilitated. The controller is obtained by implementing this important characteristic because in other way, the quaternion NN controller would not be implementable for real physical system applications.

#### 4.1 Stabilization of a port-Hamiltonian system with quaternion-based NNs

The stabilization is achieved by selecting a suitable control law obtained by selecting an appropriate Lyapunov functional, as appears in the following theorem:

**Theorem 1.** System (6) is stabilized by the following control law iff:

$$u = -\{p, \mathcal{H}\} - \frac{1}{\|p\|^2} p q^T \{q, \mathcal{H}\} - \frac{1}{\|p\|^2} p z^{rT} \left[ -A_c z^r + \sum_{r=1}^n d_{pr} f_c^r(z) + Kp \right] \\ - \frac{1}{\|p\|^2} p z^{iT} \sum_{r=1}^n d_{pr} f_c^i(z) - \frac{1}{\|p\|^2} p z^{jT} \sum_{r=1}^n d_{pr} f_c^j(z) - \frac{1}{\|p\|^2} p z^{kT} \sum_{r=1}^n d_{pr} f_c^k(z) - Rp, \quad (10)$$

where the NN controller input  $I_c = Kp$  for  $K \in \mathbb{R}^{n \times n}$  is the input gain.  $z \in \mathbb{R}^2$  is the quaternion controller input variable.

**Proof.** Consider the following Lyapunov functional:

$$V = \frac{1}{2} z^{rT} z^r + \frac{1}{2} z^{iT} z^i + \frac{1}{2} z^{jT} z^j + \frac{1}{2} z^{kT} z^k + \frac{1}{2} q^T q + \frac{1}{2} p^T p. \quad (11)$$

The derivative of the previous Lyapunov functional is obtained as follows:

$$\dot{V} = z^{rT} \dot{z}^r + z^{iT} \dot{z}^i + z^{jT} \dot{z}^j + z^{kT} \dot{z}^k + q^T \dot{q} + p^T \dot{p}, \quad (12)$$

yielding

$$\dot{V} = z^{rT} \left[ -A_c z^r + \sum_{r=1}^n d_{pr} f_c^r(z) + Kp \right] + z^{iT} \sum_{r=1}^n d_{pr} f_c^i(z) + z^{jT} \sum_{r=1}^n d_{pr} f_c^j(z) \\ + z^{kT} \sum_{r=1}^n d_{pr} f_c^k(z) + q^T \{q, \mathcal{H}\} + p^T \{p, \mathcal{H}\} + p^T u. \quad (13)$$

Now, substituting (10) into the previous equation yields

$$\dot{V} = -p^T R p. \quad (14)$$

So the system is globally asymptotically stable, and the proof is complete.  $\square$

#### 4.2 Trajectory tracking of a port-Hamiltonian system by quaternion-based NN

Taking into consideration that the trajectory tracking control for PH systems is important in many real systems, in this subsection, it is evinced the synthesis of these kinds of controllers. First as explained earlier, the quaternion NN is divided into four parts in order to obtain a feasible mathematical model for controller synthesis. The error variables for the position  $q$  and momentum  $p$  reduce the tracking error to zero. In this way, variables such as position, angular velocity, and currents can be stabilized following a predefined trajectory. It is important to remark that the Lyapunov stability theory is implemented in this research study

to synthesize the appropriate control law. For the trajectory tracking of a port-Hamiltonian dynamic system, consider the following two error variables:

$$\begin{aligned} e_1 &= q_r - q, \\ e_2 &= p_r - p \end{aligned} \quad (15)$$

where  $q_r$  and  $p_r$  are the respective references for the position and momentum. The following theorem evinces that the system is globally closed-loop stable.

**Theorem 2.** *The following control law makes the error dynamics (15) asymptotically stable iff:*

$$\begin{aligned} u = & -\{p, \mathcal{H}\} + \dot{p}_r + Q_2^{-1} \frac{1}{\|e_2\|^2} e_2 e_1^T Q_1 \dot{e}_1 + Q_2^{-1} \frac{1}{\|e_2\|^2} e_2 z^{kT} \sum_{r=1}^n d_{pr} f_c^k(z) + Q_2^{-1} \frac{1}{\|e_2\|^2} e_2 z^{jT} \sum_{r=1}^n d_{pr} f_c^j(z) \\ & + Q_2^{-1} \frac{1}{\|e_2\|^2} e_2 z^{iT} \sum_{r=1}^n d_{pr} f_c^i(z) + Q_2^{-1} \frac{1}{\|e_2\|^2} e_2 z^{rT} \left[ -A_c z^r + \sum_{r=1}^n d_{pr} f_c^r(z) + Kp \right] + Q_2^{-1} e_2, \end{aligned} \quad (16)$$

for the NN input  $I_c = Kp$ , in which  $I_c$  is the momentum state feedback, with gain matrices  $K, Q_1, Q_2$ ; in which all these matrices are positive definite. The NN is embedded in the control law in order to select the required weight values in order to stabilize the closed-loop system by making it asymptotically globally stable.

**Proof.** Consider the following:

$$V = \frac{1}{2} z^{rT} z^r + \frac{1}{2} z^{iT} z^i + \frac{1}{2} z^{jT} z^j + \frac{1}{2} z^{kT} z^k + \frac{1}{2} e_1^T Q_1 e_1 + \frac{1}{2} e_2^T Q_2 e_2. \quad (17)$$

Now, the derivative of the previous Lyapunov functional is given by

$$\begin{aligned} \dot{V} = & z^{rT} \left[ -A_c z^r + \sum_{r=1}^n d_{pr} f_c^r(z) + Kp \right] + z^{iT} \sum_{r=1}^n d_{pr} f_c^i(z) + z^{jT} \sum_{r=1}^n d_{pr} f_c^j(z) + z^{kT} \sum_{r=1}^n d_{pr} f_c^k(z) + e_1^T Q_1 \dot{e}_1 \\ & + e_2^T Q_2 [\dot{p}_r - \{p, \mathcal{H}\} - u]. \end{aligned} \quad (18)$$

Now, substituting the control law (16) into the previous equation yields

$$\dot{V} = -e_2^T e_2. \quad (19)$$

So the proof is complete, and the system is asymptotically stable.  $\square$

## 5 Experiments

For experimental purposes, the following Hamiltonian that represents a particle movement is presented as follows:

$$\mathcal{H} = \frac{1}{2m} p^T p + \frac{1}{2} k q^T q. \quad (20)$$

So by the implementation of the Poisson bracket, the representation is obtained as follows:

$$\begin{aligned} \{p, \mathcal{H}\} &= -\frac{\partial \mathcal{H}}{\partial q} - D \frac{\partial \mathcal{H}}{\partial p} = -\frac{1}{2} k q - D \frac{1}{2m} p, \\ \{q, \mathcal{H}\} &= \frac{1}{2m} p, \end{aligned} \quad (21)$$

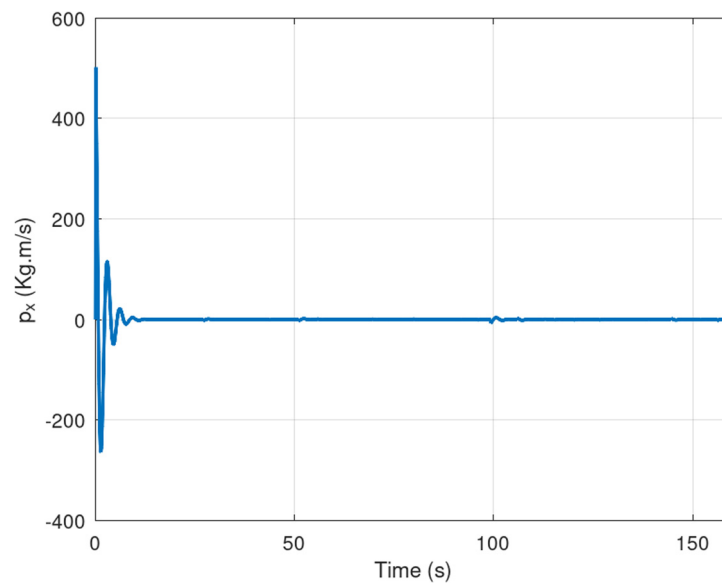
where  $D$  is the identity matrix of appropriate dimensions.

## 5.1 Experiment 1: Stabilization

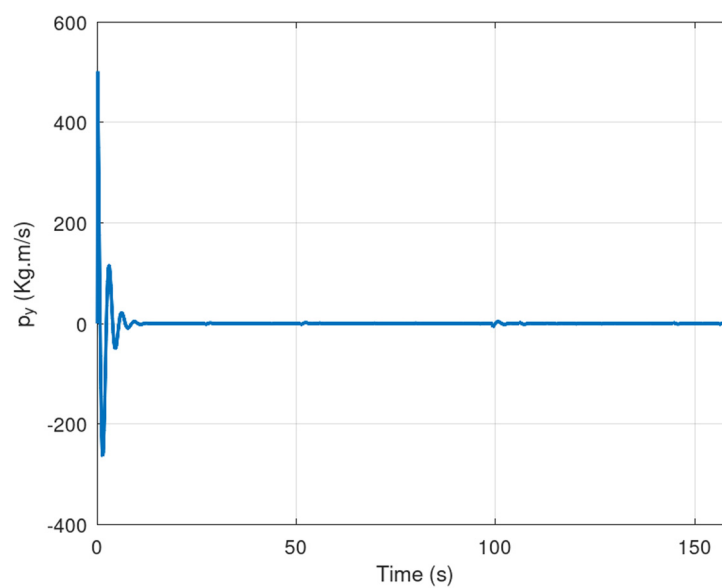
In the following experiment, the results of the stabilization of a PH system by quaternion-based NNs are presented. Consider the following value for the gain:

$$K = \begin{bmatrix} 100,000 & 0 \\ 0 & 100,000 \end{bmatrix}. \quad (22)$$

In Figures 1 and 2, the stabilized variables of the PH system for the momentum are evinced in order to observe the evolution in time for the momentum variables in the  $x$  and  $y$  axis. As can be noted the momentum reaches the origin in finite time. As it is verified later, it can be corroborated that the variables can be



**Figure 1:** Momentum  $p_x$  for Experiment 1.



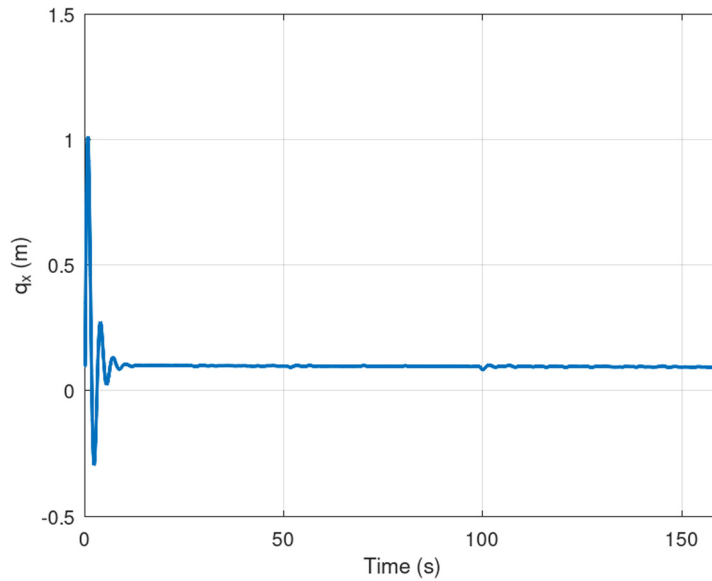
**Figure 2:** Momentum  $p_y$  for Experiment 1.



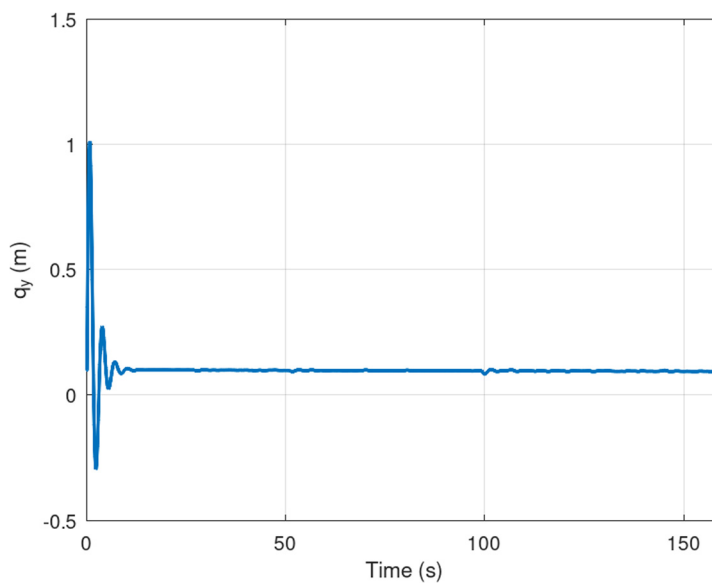
stabilized independently of the initial conditions. It is verified that there is some chattering between 50 and 100 s; the reason is as it is observed the gains ensure only global asymptotic stability due to the positive definiteness. In order to improve performance in the future, optimization algorithms will be implemented.

Meanwhile, in Figures 3 and 4, it is evinced the evolution in time of the position variables for the  $x$  and  $y$  position of the particle. Similar to the momentum variable, it is observed how the variables reach the origin in finite time, proving that the quaternion-based controller stabilizes the system variables.

Meanwhile, in Figures 5 and 6, the control effort input is shown, and as it is verified, the control effort drives the system variables to the origin in finite time. The action of the controller provides the sufficient control effort in order to drive the position and momentum variable to zero.



**Figure 3:** Position  $q_x$  for Experiment 1.



**Figure 4:** Position  $q_y$  for Experiment 1.

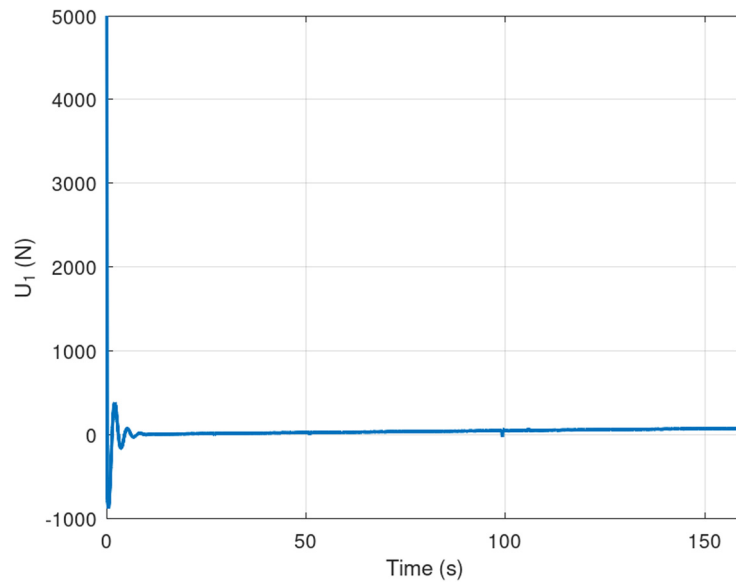


Figure 5: Input variable  $U_1$ .

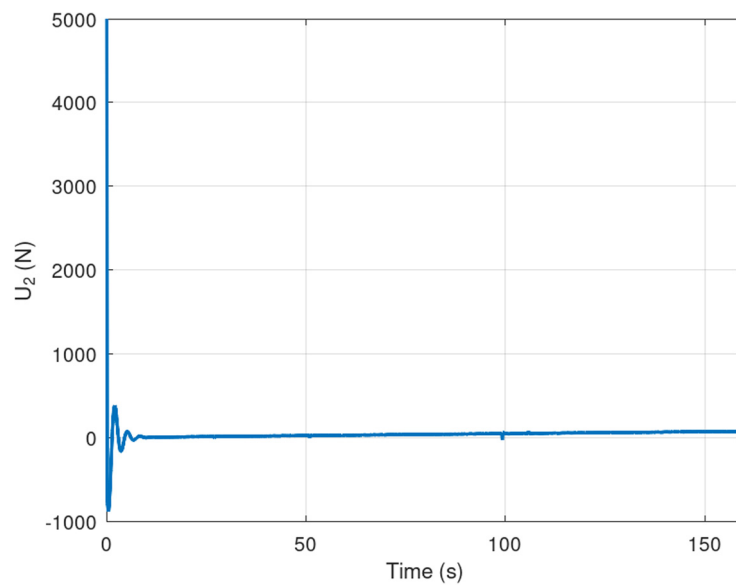


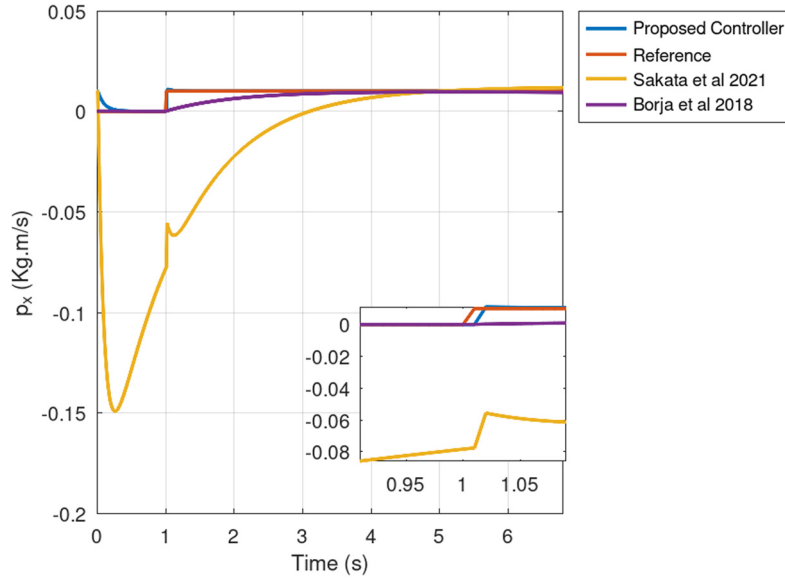
Figure 6: Input variable  $U_2$ .

## 5.2 Experiment 2: trajectory tracking

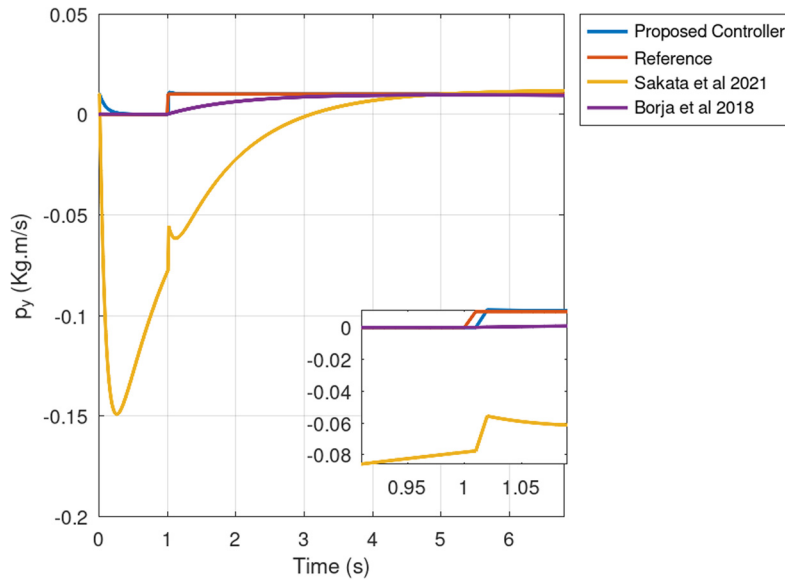
In this section, the trajectory tracking of a port-Hamiltonian system is presented in order to drive the reference variables to the final desired value in finite time and the results obtained with the proposed controller are compared with [58,68]. The parameter gains for this simulation setup are given by

$$K = \begin{bmatrix} 1 \times 10^{-8} & 0 \\ 0 & 1 \times 10^{-8} \end{bmatrix} \quad Q_1 = \begin{bmatrix} 1 \times 10^{-5} & 0 \\ 0 & 1 \times 10^{-5} \end{bmatrix} \quad Q_2 = \begin{bmatrix} 1 \times 10^{-1} & 0 \\ 0 & 1 \times 10^{-1} \end{bmatrix}. \quad (23)$$

In Figures 7 and 8, the evolution in time of the momentum in the  $x$  and  $y$  axis is presented. It is verified that the variables reach the desired value in finite time, despite the initial condition of the system. This final



**Figure 7:** Momentum  $p_x$  for Experiment 2.



**Figure 8:** Momentum  $p_y$  for Experiment 2.

value is achieved by selecting appropriate gain matrices in order to make the system stable, so the variables reach the desired final value. It is verified that the time response yielded by the proposed controller is better in comparison with the strategies shown in [58,68]

Meanwhile, in Figures 9 and 10 are presented the results of the evolution in time of the control inputs  $U_1$  and  $U_2$  in order to evince how these control input variables vary only in the transition of the reference signal value, while keeping the value in zero when the desired final value is reached. It is also verified that the control effort is smaller with the proposed control strategy in comparison with the strategies [58,68].

Finally, in Figure 11, the evolution in time of the quaternion-valued NN controller are presented for the scalar and vectorial part of the quaternion. It is verified how this quaternion-valued NN reaches the final value in finite time.

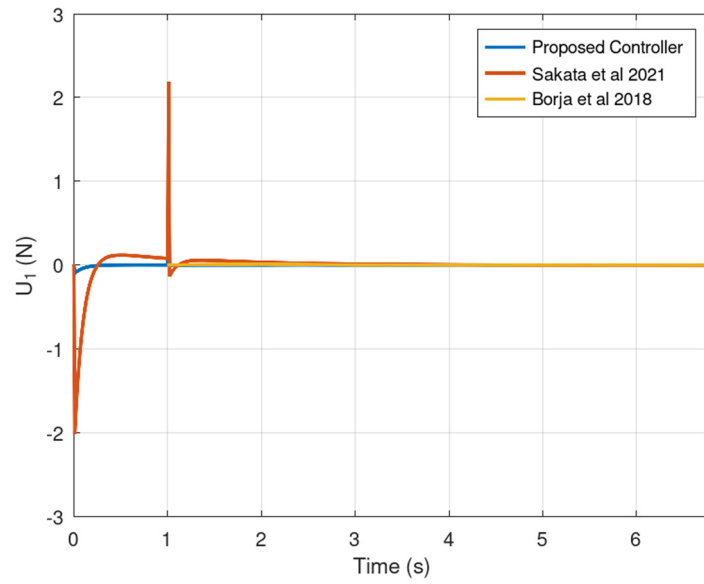


Figure 9: Input  $U_1$  for Experiment 2.

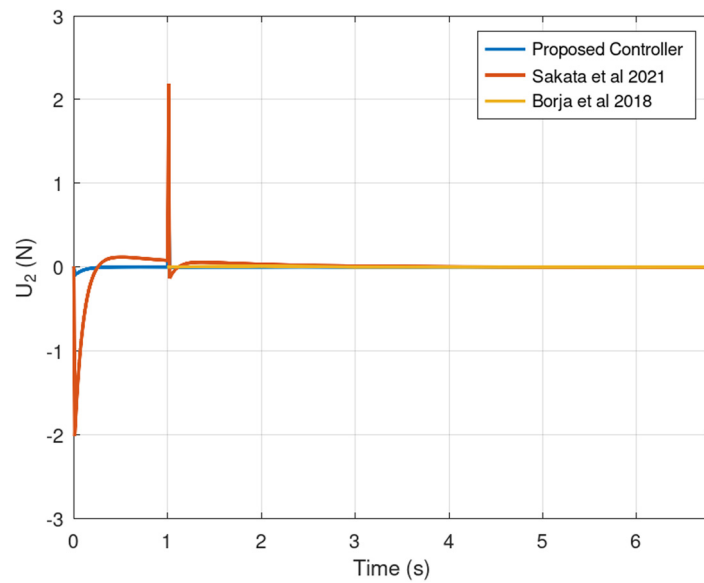


Figure 10: Input  $U_2$  for Experiment 2.

### 5.3 Experiment 3: Angular velocity trajectory tracking of an induction machine

Consider the following dq transformation for a three-phase electric motor [69]:

$$T_{abc} = \frac{2}{3} \begin{bmatrix} \cos(\theta_s) & \cos\left(\theta_s - \frac{2*\pi}{3}\right) & \cos\left(\theta_s + \frac{2*\pi}{3}\right) \\ \sin(\theta_s) & \sin\left(\theta_s - \frac{2*\pi}{3}\right) & \sin\left(\theta_s + \frac{2*\pi}{3}\right) \\ \frac{1}{2} & \frac{1}{2} & \frac{1}{2} \end{bmatrix}, \quad (24)$$

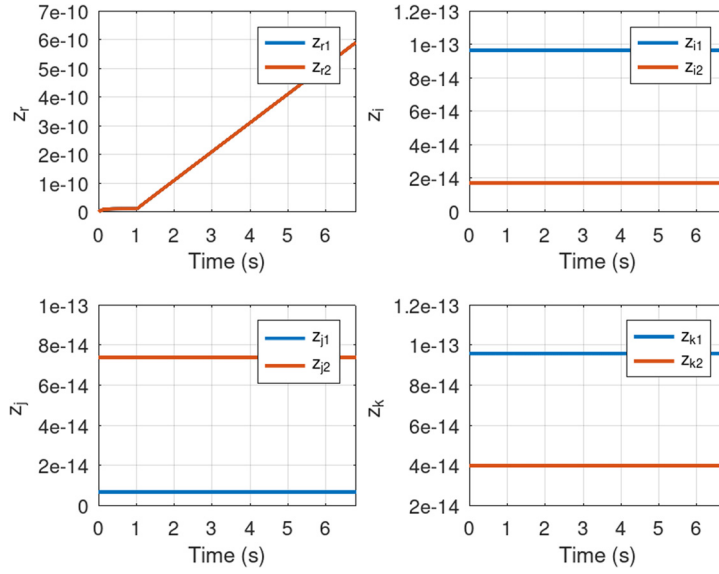


Figure 11: Quaternion-based variable  $z$  for Experiment 2.

in which in synchronous rotating reference frame is  $\omega_c = \omega_s = 2\pi f$  in which  $f = 60$  Hz. The voltages are converted to the  $d$ - $q$  axis by the following:

$$\begin{bmatrix} v_{qs} \\ v_{ds} \\ v_o \end{bmatrix} = T_{abc} \begin{bmatrix} v_{as} \\ v_{bs} \\ v_{cs} \end{bmatrix}, \quad (25)$$

in which the three-phase voltages used in the numerical experiment have an source amplitude of  $V_A = \frac{200}{\sqrt{3}}\sqrt{2} = 163.3v$  [69]. The model in synchronous reference frame of this induction machine is given by [69]

$$\begin{bmatrix} v_{qs} \\ v_{ds} \\ v_{qr} \\ v_{dr} \end{bmatrix} = \begin{bmatrix} R_s + L_s p & \omega_s L_s & L_m p & \omega_s L_m \\ -\omega_s L_s & R_s + L_s p & -\omega_s L_m & L_m p \\ L_m p & (\omega_s - \omega_r) L_m & R_r + L_r p & (\omega_s - \omega_r) L_r \\ -(\omega_s - \omega_r) L_m & L_m p & -(\omega_s - \omega_r) L_r & R_r + L_r p \end{bmatrix} \begin{bmatrix} i_{qs} \\ i_{ds} \\ i_{qr} \\ i_{dr} \end{bmatrix}, \quad (26)$$

with the respective voltages and currents as specified in [69].  $R$ ,  $L$ ,  $p$ , and  $\omega_r$  indicate the resistances, inductances, number of poles, and rotor angular velocity, respectively. The parameter values for this numerical experiment are [69] 5 hp, 200 v, three-phases, 60 Hz, 4 poles, star connected,  $R_s = 0.277\Omega$ ,  $R_r = 0.183\Omega$ ,  $L_m = 0.0538$  H,  $L_s = 0.0553$  H, and  $L_r = 0.056$  H.

Consider the following state vector  $Q = [i_{qs}, i_{ds}, i_{qr}, i_{dr}, \omega_r]$  with the following inductance-inertia matrix:

$$L = \begin{bmatrix} M & 0 \\ 0 & J \end{bmatrix}, \quad (27)$$

where  $J$  is the motor inertia and the matrix  $M$  is

$$M = \begin{bmatrix} L_s & 0 & 0 & 0 \\ 0 & L_s & 0 & 0 \\ 0 & 0 & L_r & 0 \\ 0 & 0 & 0 & L_r \end{bmatrix}. \quad (28)$$

Consider the following Hamiltonian

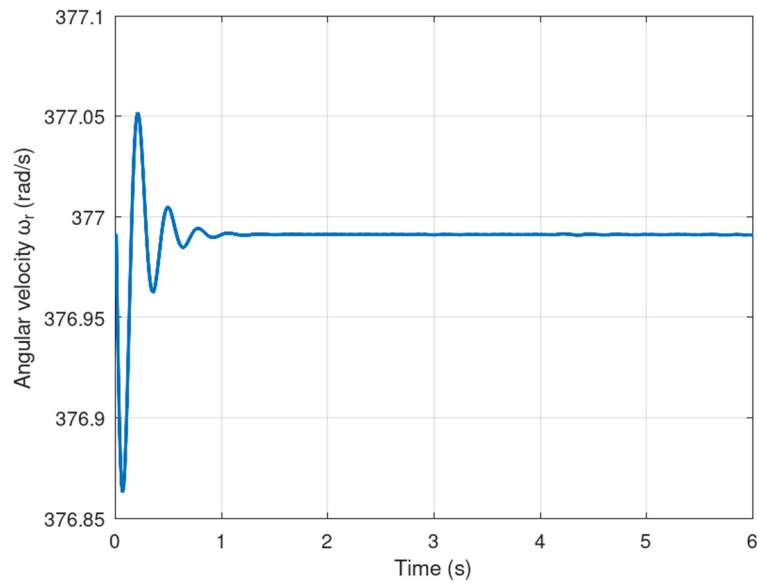
$$\mathcal{H} = \frac{1}{2} p^T L^{-1} p + \frac{1}{2} Q^T L Q, \quad (29)$$

in which  $p \in \mathbb{R}^5$  is the momentum vector. The PH representation is given by:

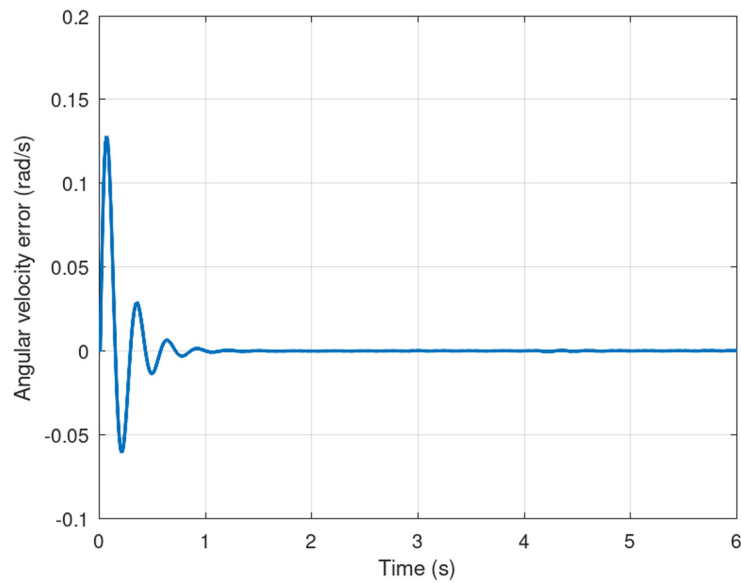
$$\begin{aligned}\dot{q} &= \{q, \mathcal{H}\}, \\ \dot{p} &= \{p, \mathcal{H}\} + U_1,\end{aligned}\tag{30}$$

with the following operators:

$$\begin{aligned}\{p, \mathcal{H}\} &= -LQ - DL^{-1}P, \\ \{q, \mathcal{H}\} &= L^{-1}P,\end{aligned}\tag{31}$$



**Figure 12:** Rotor angular velocity.



**Figure 13:** Rotor angular velocity error.

where  $D = I_5$  is an identity matrix of appropriate dimensions with the input vector given by:

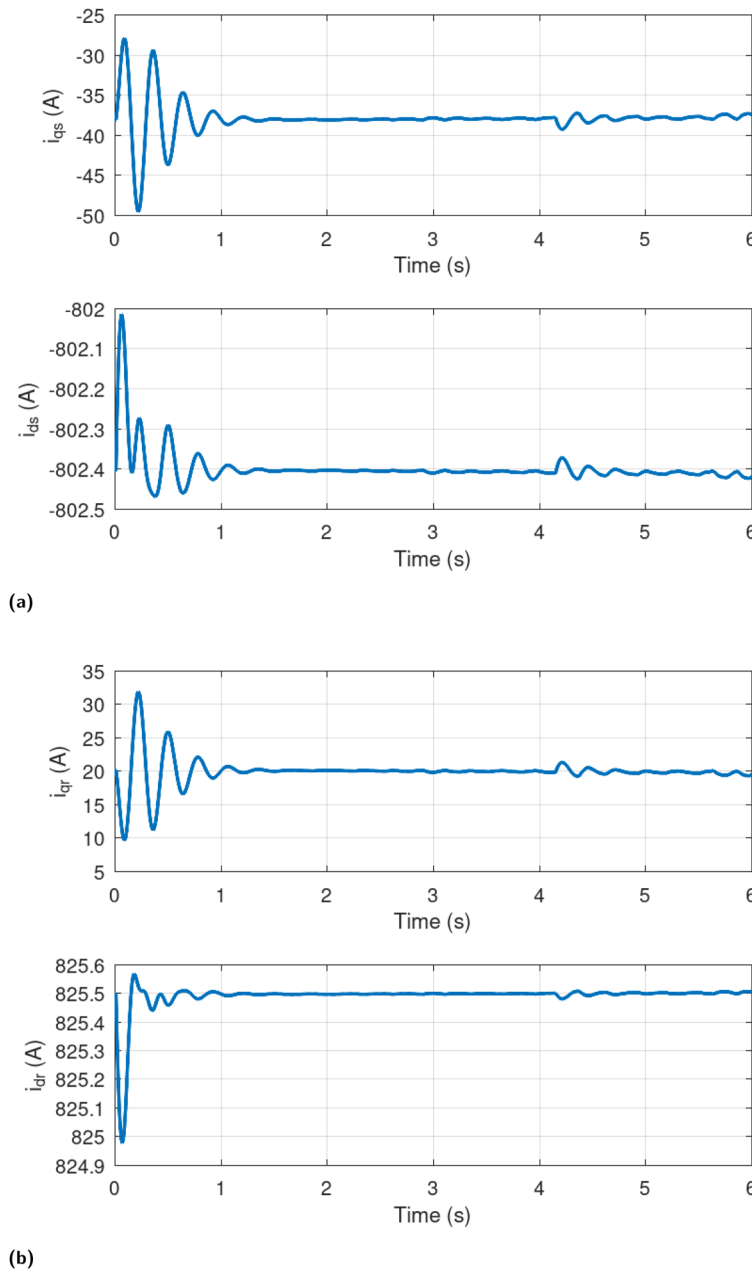
$$U_1 = \begin{bmatrix} U \\ T_e - T_L \end{bmatrix}, \quad (32)$$

where  $T_L$  is the torque generated by the motor load and  $T_e$  is given by [69]:

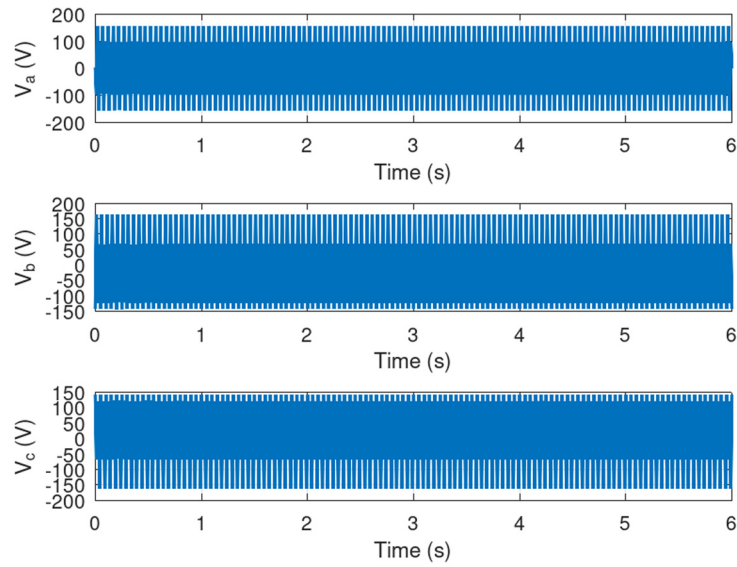
$$T_e = \frac{3p}{2} L_m (i_{qs} i_{dr} - i_{ds} i_{qr}). \quad (33)$$

For this numerical experiment, a torque load  $T_L = 1 \text{ N} \times \text{m}$  is applied at 0 s with a load inertia of  $L = 200 \text{ kg} \times \text{m}^2$ . The parameters of the neural-network controller are given by  $K = 70 \times I_5$ ,  $Q_1 = Q_2 = 0.1 \times I_5$ .

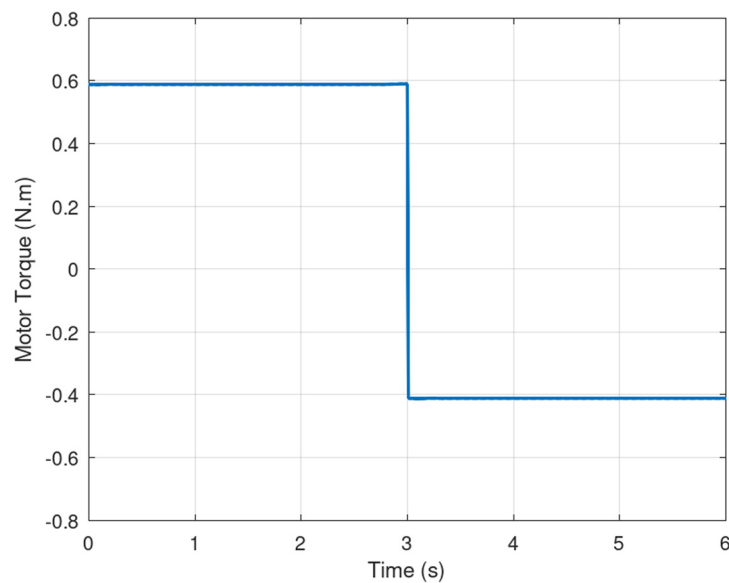
In Figures 12 and 13, the angular velocity of the motor rotor is depicted with the respective error. It is noted how the angular velocity reaches the synchronous speed in finite time by driving the error to zero.



**Figure 14:** Stator and rotor currents. (a)  $i_s$  in the d-q axis and (b)  $i_r$  in the d-q axis.



**Figure 15:** Input voltages for the  $a$ ,  $b$ , and  $c$  phases.



**Figure 16:** Motor torque.

Meanwhile, in Figure 14, the currents are shown evincing that the currents reach the steady-state value in finite time.

Finally, in Figures 15 and 16 are shown the three-phase input voltages along with the motor torque as they vary in time.

## 6 Results and discussion

In this section, the discussion of the theoretical and experimental results of this research study is presented in order to analyze its contributions. As shown in the theoretical part of this research study, first the PH system is simplified by the implementation of a Poisson bracket in order to synthesize the derivation of the NN



controller. The Poisson brackets allow us to obtain the port-Hamiltonian formulation, and at the same time, it provides a compact representation of these kinds of systems. In this research study is only considered that the port-Hamiltonian system is for one and multi-particle systems; in other words, these can be implemented for the representation by port-Hamiltonian systems that model the dynamics of electrical, mechanical, molecular, and diverse types of physical systems.

In the case of the numerical experiment simulation, it is verified efficiently how the port-Hamiltonian system is stabilized taking into account the dynamics of a particle. It is important to note that the quaternion NN controller stabilizes the position and the momentum variable. The quaternion NN controller acts as a stabilizer for this system taking into consideration the dynamic properties of this port-Hamiltonian system. Apart, the proposed port-Hamiltonian system is driven to a final desired value using a reference trajectory taking into consideration the flexibility of a quaternion NN controller by selecting the appropriate gain matrices, the system position, and momentum variables to the final desired variables. With these numerical experiments, the derivation of NN control laws by the selection of appropriate Lyapunov functions is verified.

## 7 Conclusion

In this research study, the derivation of a stabilizer and a trajectory tracking control law is shown, based on a quaternion-based NN. It is important to consider that in both cases, the quaternion-based NN is divided into the scalar and vectorial quaternion part, in order to obtain the suitable control laws in order to drive the system variables, the momentum and position variables, to the final desired value in finite time. It is important to take into consideration that the Poisson brackets are implemented in order to simplify the mathematical deductions taking into consideration that the mathematical derivations of the port-Hamiltonian mathematical formalism are compact and simple. By means of two numerical examples, the theory shown in this article is verified and validated. The control laws are obtained by selecting suitable Lyapunov functionals in order to make the system stable. It is important to clarify that the theoretical results obtained in this research study were compared with passivity-based strategies, taking into consideration that energy-based controllers are commonly designed to control and stabilizes port-Hamiltonian systems. The experimental results prove that the proposed control strategy yields a better closed-loop performance in comparison with passivity-based control due to a better time response.

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